



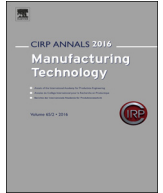
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# Cooling capability of liquid nitrogen and carbon dioxide in cryogenic milling

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## ABSTRACT

This paper discusses an investigation into the capability of liquid nitrogen (LN<sub>2</sub>) and liquid carbon dioxide (LCO<sub>2</sub>) as a coolant in machining. A comparative analysis of the heat-transfer rate was made utilizing cooling of a controlled heat source with an integrated temperature sensor. The analysis was coupled with experimental in-process temperature measurements in cryogenic milling of titanium alloy Ti-6Al-4V (β). The results indicate that cooling capability differs between these two cryogenic media, in both the observed cooling rate as well as in the achieved steady-state temperature.

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## 1. Introduction

Liquid nitrogen (LN<sub>2</sub>) and liquid carbon dioxide (LCO<sub>2</sub>) are the two most commonly used cryogenic media for machining applications [1]. However, the differences between LN<sub>2</sub> and LCO<sub>2</sub> in terms of delivery conditions into the cutting zone, as well as in their cooling capability (ability for heat extraction during the machining process), are not well understood. A quantitative measure of the ability of a cryogen to remove a certain amount of heat from the cutting zone refers to heat-transfer rate in Watts [2]. In previous studies, the cooling capability of cryogenic media was estimated via the determination of the heat-transfer coefficient between the cryogenic media and the workpiece surface. It was found that heat evacuation is proportional to the coefficient of heat transfer and the difference between the cryogenic media temperature and the contact surface temperature [3–6]. In addition, cooling capability was also estimated with temperature measurements during or after the machining process [7–10]. However, in observing the results, huge variations with contradictory trends can be observed. Furthermore, there is a lack of fundamental studies – employing a direct determination of the cooling capability of LN<sub>2</sub> and LCO<sub>2</sub>, as well as their comparison in terms of the cooling rate and the achieved steady-state temperature – in comparison to conventional cooling with emulsion.

Considering this, an attempt is made to advance the understanding of the cooling heat-flow rate of LN<sub>2</sub> and LCO<sub>2</sub>. Their cooling capabilities are compared with the cooling capability of standard conventional cooling with emulsion. First, heat-evacuation mechanisms for LN<sub>2</sub> and

LCO<sub>2</sub> are briefly discussed, followed by a fundamental cooling-capability assessment using a controlled heat source with an integrated temperature sensor. With this method, it is possible to determine the cooling heat flow rate, expressed in Watts, for all coolants, as well as the maximum cooling rate, measured in °C/s. The experiments were verified via measurements of the in-process cutting temperature using embedded thermocouples in the cutting inserts during milling of titanium alloy Ti-6Al-4V (β).

## 2. Heat-evacuation mechanisms

In conventional machining (cooling with emulsion), an emulsion is delivered into the cutting zone at ambient temperature. In this situation, the heat evacuation mechanism, as well as related cooling capability, is largely dependent on the temperature difference. The sensible heat transfer rate,  $Q'_s$ , in W is:

$$Q'_s = \dot{m} \cdot c_p \cdot (T_{m2} - T_{m1}) \quad (1)$$

where  $\dot{m}$  is the media mass flow rate, in kg/s,  $c_p$  the specific heat capacity, in J/kg K;  $T_{m1}$  the media temperature before entering the cutting zone, in °C, and  $T_{m2}$  media temperature when leaving the cutting zone, in °C. The LN<sub>2</sub> is stored in the vacuum-insulated Dewar, usually under a pressure of 4 bar (0.4 MPa) and delivered through the insulated piping into the cutting zone at −195.8 °C (77.35 K). When the LN<sub>2</sub> hits the higher-temperature workpiece surface, it evaporates from the contact area. Due to the temperature difference and phase transformation of the nitrogen (from liquid to gas), there is convective heat transfer from the tool to the nitrogen, resulting in a temperature decrease in the tool. The total heat capability is therefore the sum of the sensible heat transfer rate (Eq. (1)) and latent heat transfer rate,  $Q'_l$ , in W which is

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due to the phase transformation from liquid to gas, determined by:

$$Q'l = \cdot h_e \quad (2)$$

where  $h_e$  is the latent heat of vaporization, in J/kg. On the other hand, LCO<sub>2</sub> is stored and delivered into the cutting zone at an ambient temperature, e.g. 20 °C (293.15 K) and a pressure of 57 bar (5.7 MPa). Due to the decrease of the saturation pressure upon exiting the nozzle, the LCO<sub>2</sub> vaporizes and expands, absorbing heat from the surroundings. This is caused based on evaporation, Joule–Thompson and sublimation mechanisms. If the amount of LCO<sub>2</sub> is sufficient, the micro-region is cooled down to the boiling point of CO<sub>2</sub>, –78.5 °C (194.65 K). Therefore, the total heat capability of LCO<sub>2</sub> can be determined similarly as for LN<sub>2</sub> [1,2,11]. However, it must be noted that not all of the latent heat generated due to the phase transformation of LN<sub>2</sub> or LCO<sub>2</sub> is used to cool the cutting zone. Some portion is also consumed in the surroundings. The impact of the surrounding is visible in Fig. 1, where the temperatures of the emulsion, the LN<sub>2</sub> and the LCO<sub>2</sub> are measured (detailed explanation of the experimental setup in Section 3). Measurements were performed with thermocouples placed just before entering and when leaving the heating zone.

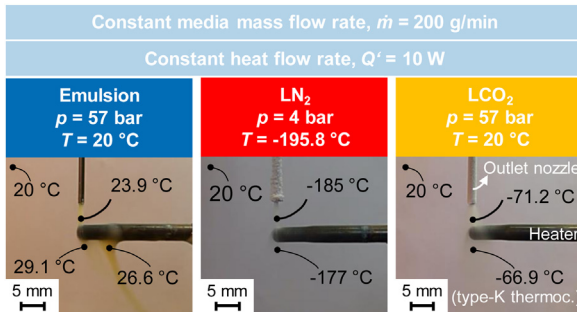


Fig. 1. Comparative temperatures of the media before cooling and right after leaving the hot zone of a controlled heat source.

### 3. Fundamental experiments

For the fundamental experiments, a unique experimental setup was developed, as shown in Fig. 2. A controlled heat source (heater) was used for constant heat generation simulating the heat generation in machining process. By varying the input power, in Watts, different rates of heat generation were achieved. Furthermore, the temperature inside the heater was monitored using an integrated type-K thermocouple with a sampling rate of 200 ms. The emulsion, LN<sub>2</sub> and LCO<sub>2</sub> were delivered to the heater via an outlet nozzle with the diameter of  $d = 0.8$  mm. The heat-source power was varied in order to achieve controlled heater temperatures of 50 °C (323.15 K), 80 °C (353.15 K), 100 °C (373.15 K) and 200 °C (473.15 K). In this way, the cooling capability of a delivered media is directly correlated to the heat transfer rate of the heater.

Afterwards, the maximal cooling rate of the media was determined by observing the temperature drop of heater from 100 °C (373.15 K), when the heater was turned OFF. The derivative of temperature signals have been analyzed in time and the maximal cooling rate has been calculated as average of five points of derivative, where maximum exists. An emulsion with a 7% concentration was supplied using a high-pressure (HP) pump from the emulsion tank of the machining center under the same temperature and pressure as the LCO<sub>2</sub>, which was stored in a bottle at 20 °C (293.15 K) and 57 bar (5.7 MPa). LN<sub>2</sub> was supplied from the Dewar under a pressure of 4 bar (0.4 MPa) and temperature of –195.8 °C (77.35 K). The mass flow rate of all the media was set constant during each experiment. Experiments were performed for two different flow levels: 100 and 200 g/min, determined from Refs. [7,12]. The emulsion and LCO<sub>2</sub> mass flow rates were controlled using a precision needle valve and Coriolis mass flow meter. For the LN<sub>2</sub> mass flow rate control, a weighting of the Dewar and a proprietary SUSCRYMAC delivery system were used. All experiments utilized the same outlet nozzle with an inner diameter of 0.8 mm. The nozzle was positioned 5 mm from the heater, which represents a comparable distance between the exit nozzle and the cutting insert of the milling tool used for the milling experiments in this study (presented in Section 4). The center of the outlet nozzle was aligned with the center of the heater, which is 1 mm from the heater's edge, as shown in Fig. 2. Furthermore, two nozzle angles were investigated: (a) Nozzle position A with a projection angle of 60° was selected in order to exclude the impact of the wettability of the medium on the heater's surface, as performed in Ref. [13], and (b) orthogonal Nozzle position B with a projection angle of 90°, which was found by Refs. [1,14] to be the most effective for cooling. For the sake of repeatability, each experiment was repeated 4 times.

Fig. 3 shows the cooling heat transfer rates of emulsion, LN<sub>2</sub> and LCO<sub>2</sub>. It is evident that the cooling capability of emulsion, LN<sub>2</sub> and LCO<sub>2</sub> increases with increasing media mass flow rate. For experiments with nozzle position A (60° projection angle), the cooling capability of LN<sub>2</sub> and LCO<sub>2</sub> – with the same mass flow rate – is comparable. However, due to its higher heat of vaporization, LCO<sub>2</sub> has a slightly higher cooling heat-transfer rate than LN<sub>2</sub>. In addition, the heat evacuation mechanism of LN<sub>2</sub> and LCO<sub>2</sub> is mainly dependent on their phase transformation and heat absorption, therefore, the cooling capability of LN<sub>2</sub> and LCO<sub>2</sub> slowly increases with an increase in workpiece temperature and is mainly conditioned by the media flow rate. Knowing this, it can be seen, that with a controlled media mass flow rate, the cutting temperature can be controlled or even optimized [15]. In contrast, the heat-evacuation mechanism of emulsion is mainly dependent on the temperature difference, meaning that the cooling capability of emulsion increases when a higher heat-transfer rate is generated on the heater. Therefore, the cooling capability of emulsion at a lower workpiece temperatures is reduced, compared to the cooling capabilities of LN<sub>2</sub> and LCO<sub>2</sub>. Similar findings can be observed when experimenting with an orthogonal nozzle position

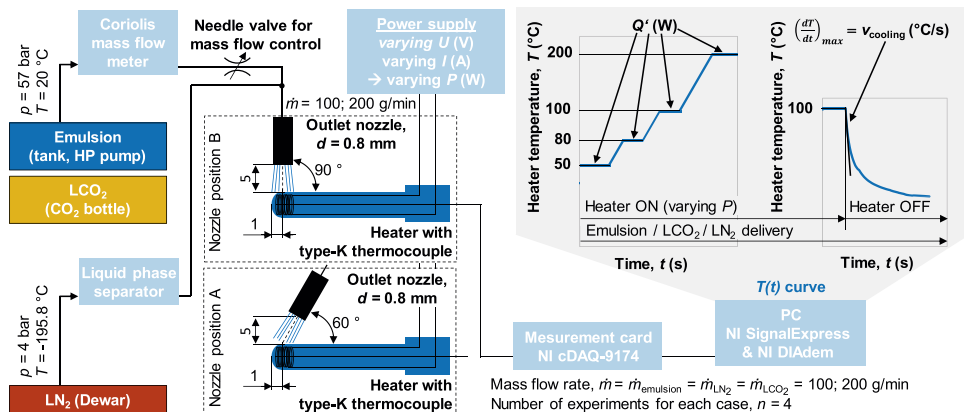


Fig. 2. Illustration of the experimental setup for fundamental experiments.

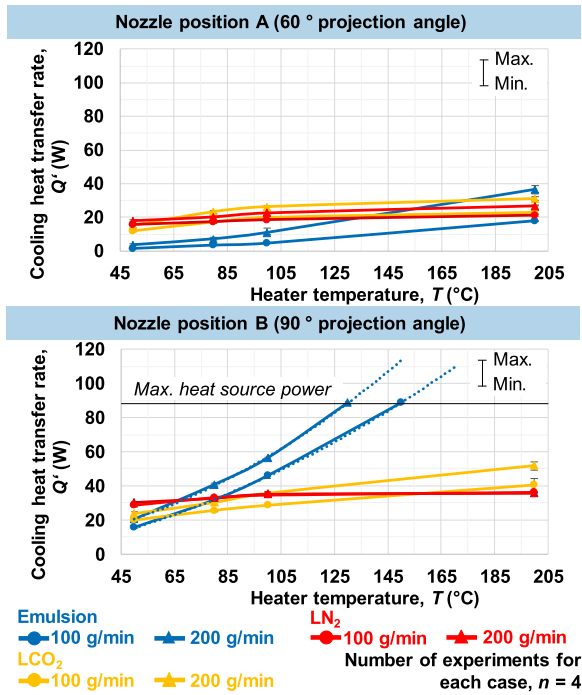


Fig. 3. Cooling heat transfer rates of emulsion, LN<sub>2</sub> and LCO<sub>2</sub>.

B (90° projection angle). Here, due to the direct impact of the media onto the heater, an overall higher cooling capability of emulsion, LN<sub>2</sub> and LCO<sub>2</sub> can be observed. Similar trends have been observed in Refs. [1,14], where the authors found that the orthogonal orientation of the tool cooling channel relative to the cutting edge is the most effective for cooling of the cutting zone. In addition, good wettability is essential for effective cooling [16]. The emulsion remains in liquid phase during cooling, therefore it stays in contact with the heater's surface for a longer time. Moreover, it can be seen that the surface area affected by the emulsion is much larger than the area affected by LN<sub>2</sub> or LCO<sub>2</sub> (visible on Fig. 1). Therefore, the emulsion offers better overall bulk cooling in comparison to LN<sub>2</sub> and LCO<sub>2</sub>. However, when considering the maximum cooling rates, similar results can be seen for emulsion, LN<sub>2</sub> and LCO<sub>2</sub> (Fig. 4).

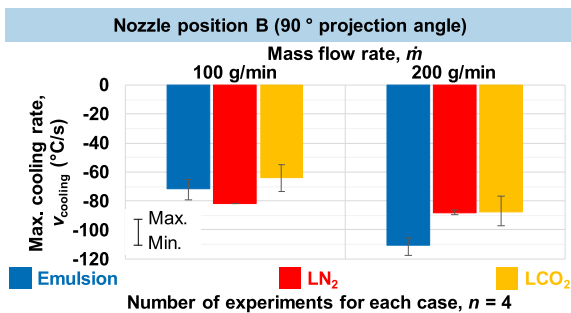


Fig. 4. Maximum cooling rates of emulsion, LN<sub>2</sub> and LCO<sub>2</sub>.

#### 4. Milling experiments

In order to verify the fundamental experiments, milling experiments using in-process cutting-temperature measurements were performed on two separate but comparable experimental setups. The first were performed on an industrial case study, while the second were performed with direct verification of the cooling fluid delivery principle used in the fundamental study. Titanium alloy Ti-6Al-4V in  $\beta$  microstructure was used as the workpiece material with the cutting parameters:  $v_c = 40$  m/min,  $f_z = 0.1$  mm,  $a_p = 4$  mm,  $a_e = 0.6 \times D$  mm. For the sake of repeatability, each milling experiment was repeated two times.

A Mori Seiki Frontier M three-axis CNC vertical machining center was used to perform the milling experiments under conventional cooling with emulsion and cryogenic LN<sub>2</sub> and LCO<sub>2</sub> cooling. Emulsion (7% concentration) and LCO<sub>2</sub> were supplied from inside the cutting tool through a nozzle with an 0.8 mm diameter under a pressure of  $p = 57$  bar (0.5 MPa) and temperature of  $T = 20^\circ\text{C}$  (293.15 K). Due to the low temperatures of LN<sub>2</sub> and related problems (insulation, etc.), LN<sub>2</sub> was supplied into the cutting zone from the Dewar via an outlet nozzle with a diameter of  $d = 0.8$  mm. Milling experiments were performed for two different media flow rates of  $\dot{m} = 100$  and 200 g/min, the media mass flow rate was controlled in the same way as in the fundamental experiments.

A special, tailor-made tool holder with an integrated rotary unit for through-the-tool delivery of coolant was developed. A single-tooth milling cutter with a diameter of  $D = 10$  mm with the appropriate CVD Ti(C,N)-coated tungsten-carbide insert was used. For the in-process cutting temperature measurements, a tailor-made telemetry system with type-K thermocouple with a diameter of  $d = 0.5$  mm integrated into the cutting insert was developed. The position of the thermocouple was at the tip of the tool, 0.1 mm from the rake face.

The telemetry system consists of a stationary part and a rotary part. The stationary part is used to provide an inductive power supply to the rotary part, to which the thermocouple is connected and rotates together with the cutting tool. Wireless transmission was used for the temperature data-transfer from the rotary part to a computer application that records data with a sampling rate of 20 ms. The second set of temperature measurements in milling process, using industrial state-of-the-art conditions of cooling with emulsion, were also performed and compared to the temperatures in CO<sub>2</sub>-assisted machining. In this case, emulsion was supplied under a pressure of  $p = 5$  bar (0.5 MPa) from the outside via an outlet nozzle with the diameter of 5 mm into the cutting zone with a corresponding volumetric flow rate of  $\dot{V} = 33.6$  L/min. These experiments were performed on an Ex-Cell-O XHC 241 four-axis CNC horizontal machining center with a 4-cutting-edge,  $D = 40$  mm, milling cutter of the type Cryo.tec<sup>®</sup> F4042.6903229 provided by WALTER TOOLS. The identical CVD Ti(C,N)-coated tungsten-carbide inserts and K-type thermocouple, integrated into one cutting insert, were used, as shown in Fig. 5. The LCO<sub>2</sub> mass flow rate was controlled by an AEROSOL MASTER 4000cryolub<sup>®</sup> system of ROTHER TECHNOLOGIE and a Coriolis mass flow meter. While in this case the temperature measurement data were transferred via a wireless FM/PCM transmitter produced by MANNER SENSORTELEMETRIE. The thermoelectric voltage of the thermocouple was recorded with a sample rate of 6620 Hz. Further details are presented in Ref. [17].

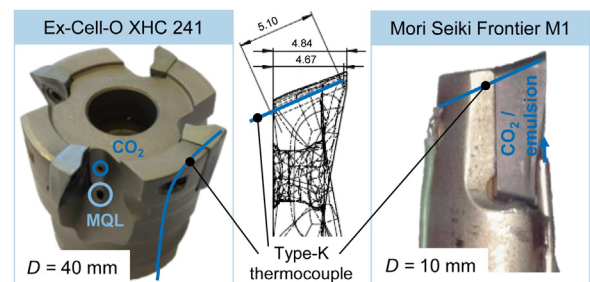


Fig. 5. Cutting tools with embedded type-K thermocouples used in milling experiments.

The results from both verification milling experiments are shown in Fig. 6. Observing the temperature results obtained during milling of titanium alloy Ti-6Al-4V ( $\beta$ ) under different cooling conditions, comparable trends can be observed, even when correlating them with temperature measurements in fundamental experiments with cooling of a known heat source. Cutting temperatures are inversely proportional to the cooling capability/cooling heat-transfer rate and the mass flow rate of a given media, i.e., the cutting temperature achieved in the presence of the



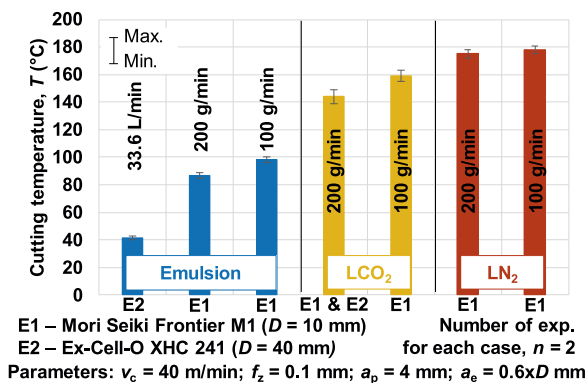


Fig. 6. Cutting temperatures during milling of titanium alloy Ti-6Al-4V (β) under different cooling conditions.

coolant with a higher cooling capability will be lower. In addition, a higher mass flow rate of a coolant will result in a lower cutting temperature. As shown in Section 3, emulsion provides better cooling capability than cryogenic media and therefore, the lowest cutting temperature was achieved under cooling with emulsion, followed by cooling with LCO<sub>2</sub> and LN<sub>2</sub>, respectively. It was found that, when using media mass flow rates of 100 and 200 g/min, emulsion provides, on average, 92% and 64% better cooling (higher heat transfer rate) compared to LN<sub>2</sub> and LCO<sub>2</sub>, respectively. However, from our previous work, it has been shown that, even though the temperatures of the process are lower with using emulsion, using LCO<sub>2</sub> in combination with MQL in milling yields longer tool life in comparison to cooling with emulsion [12]. This indicates that there exists an optimal cutting temperature which produces the longest tool life: too low of a temperature can result in a shorter tool life. Therefore, the coolant flow rate has to be controlled and optimized.

## 5. Conclusions

Cooling capabilities of LN<sub>2</sub> and LCO<sub>2</sub> were experimentally assessed by measuring in-process temperatures during fundamental heat-transfer test and verified during milling of titanium alloy Ti-6Al-4V (β). Main findings are the following:

- The cooling capability of emulsion, LN<sub>2</sub> and LCO<sub>2</sub> increased with increasing media mass flow rate.
- The coolant outlet nozzle orientation has a significant effect on a media's cooling capability. The most effective nozzle orientation is orthogonal to the heat source.
- The heat-evacuation mechanism of LN<sub>2</sub> and LCO<sub>2</sub> mainly depends on the heat absorption due to the phase transformation of the cryogen.
- Heat evacuation with emulsion is mainly dependent on the temperature difference, meaning that its cooling capability increases with heat generation, in contrast to the cryogenic media. This is because the emulsion remains in the liquid state during cooling, and therefore stays in contact with the heater or workpiece surface for a longer time.
- Cutting temperature measurements coupled with tool life experiments indicate that there exists an optimal cutting

temperature that can be achieved by sufficient mass flow rate of a coolant.

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