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# Insight into the SO<sub>2</sub> poisoning mechanism for NO<sub>x</sub> removal by NH<sub>3</sub>-SCR over Cu/LTA and Cu/SSZ-13

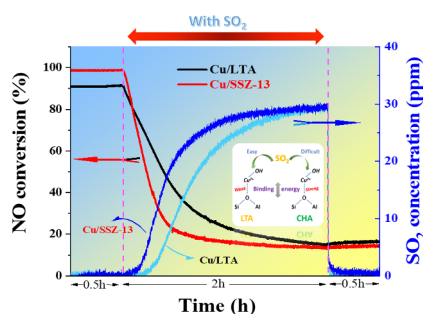
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## HIGHLIGHTS

- Cu/LTA and Cu/SSZ-13 were synthesized and examined for SO<sub>2</sub> poisoning.
- [Cu(OH)]<sup>+</sup> in Cu/LTA is found to be more vulnerable to SO<sub>2</sub> than Cu/SSZ-13.
- In SCR condition with SO<sub>2</sub>, Cu/LTA can store more SO<sub>2</sub> than Cu/SSZ-13.
- Cu/LTA exhibit a slower deactivation rate than Cu/SSZ-13.
- 750 °C fully regenerates Cu/LTA, while Cu/SSZ-13 show some loss at high temperature.

## GRAPHICAL ABSTRACT



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## ABSTRACT

In this study, Cu/LTA and Cu/SSZ-13 catalysts are examined for sulfur poisoning and regeneration. The nature of the Cu species was probed with H<sub>2</sub>-TPR and *in-situ* DRIFTS. These characterizations collectively indicate that primarily Z2Cu is present in Cu/LTA, whereas Cu/SSZ-13 contains a higher concentration of ZCuOH. ZCuOH is proved to be more vulnerable to SO<sub>2</sub> poisoning than Z2Cu sites in both Cu/zeolites. H<sub>2</sub>-TPR results suggest that the interaction of ZCuOH with the framework in Cu/LTA is much weaker than in Cu/SSZ-13, thereby leading to more susceptibility to SO<sub>2</sub> adsorption. Moreover, Cu/LTA can store more SO<sub>2</sub> under NH<sub>3</sub>-SCR conditions in the presence of SO<sub>2</sub>, and it also has a slower deactivation rate due to the different location of generated (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>. Cu/LTA can be fully restored after regeneration at 750 °C. However, Cu/SSZ-13 experiences a loss of activity at high temperature, which is attributed to newly formed CuO<sub>x</sub> clusters.

## 1. Introduction

The selective catalytic reduction (SCR) method developed in the 1970s has high efficiency and is currently the most widely used process for industrial NO<sub>x</sub> removal [1]. In this method, the reducing agents used are CO or H<sub>2</sub> [2–4], various hydrocarbons [5–7], and NH<sub>3</sub> [8–12]. The catalysts are (un)supported non-noble metal oxides (V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>/TiO<sub>2</sub>, MnO<sub>x</sub>, etc.) [13–17], supported noble metals (Ag/Al<sub>2</sub>O<sub>3</sub>, etc.) [18–20], and zeolite catalysts (Cu or Fe/BEA, CHA, FER, etc.) [21–25].

Moreover, ammonia selective catalytic reduction (NH<sub>3</sub>-SCR, 4NH<sub>3</sub> + 4NO + O<sub>2</sub> → 4N<sub>2</sub> + 6H<sub>2</sub>O) has become the primary technology for the abatement of NO<sub>x</sub> emissions from diesel engines [26,27]. The ammonia is produced through the thermal decomposition and hydrolysis of aqueous urea (CO(NH<sub>2</sub>)<sub>2</sub> + H<sub>2</sub>O → 2NH<sub>3</sub> + CO<sub>2</sub>). Copper-exchanged chabazite (CHA) framework zeolites, e.g., Cu/SSZ-13, have been extensively studied and practically applied in the last decade as NH<sub>3</sub>-SCR catalysts for NO<sub>x</sub> abatement in diesel vehicles [8,28–32]. However, with long-term exposure to harsh temperatures,

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e.g., 800 °C, which occasionally occurs for regeneration purposes, a Cu/SSZ-13 catalyst has a high risk of degradation, which leads to catalyst deactivation [33]. Hong's group [34] has recently found that high-framework silica Cu/LTA zeolite is a more robust SCR catalyst that withstands hydrothermal aging even at 900 °C and maintains remarkable NH<sub>3</sub>-SCR activity. We have confirmed this extraordinary stability and investigated the mechanism for the unusual stability of Cu/LTA catalyst [35].

Cu/zeolites adapted in the Exhaust Aftertreatment System (EATS), whether CHA or LTA framework topology, inevitably undergo sulfur (e.g., SO<sub>2</sub>) contamination because of the presence of ppm levels of sulfur (< 15 ppm) in commercial fuel, even under the Ultra-Low Sulfur Diesel (ULSD) regulation [36–39]. In-depth studies of Cu-chabazite SCR catalysts, including Cu/SSZ-13 and Cu/SAPO-34, have reported on the effect of sulfur poisoning [36,39–44]. In general, two main deactivation processes are suggested: chemical and physical. Kumar et al. [41] have investigated various effects of SO<sub>2</sub> and SO<sub>3</sub> on Cu/CHA SCR catalysts and found that the presence of SO<sub>3</sub> resulted in a large impact on catalytic performance. Similar results have also been reported by Cheng and coworkers [40], who propose that the formation of CuSO<sub>4</sub> upon SO<sub>3</sub> poisoning can be responsible for the deactivation. Several studies [38,42] are available regarding the impact of SO<sub>2</sub> on Cu/CHA catalysts (SAPO-34 or SSZ-13), and it is suggested that the formation of ammonium sulfate species may poison the active sites and also block zeolite pores. Li's group [45] have compared sulfate formation on Cu/SSZ-13 and Cu/SAPO-34 catalysts, and have found three sulfate species on the catalyst surface, i.e., H<sub>2</sub>SO<sub>4</sub>, CuSO<sub>4</sub>, and Al<sub>2</sub>(SO<sub>4</sub>)<sub>3</sub>. Wijayanti et al. [46] have also found that H<sub>2</sub>O and hydrothermal aging can significantly promote the formation of copper sulfates.

Pioneering work by Kwak et al. [47] has shown that Cu ions primarily occupy sites in the 6-membered rings at low ion exchange levels, while these ions are mostly present in the large cages of the CHA structure at high ion exchange levels. On this basis, later research [32,48] further identified that these two distinct Cu cationic species are: (1) ion-exchanged Cu<sup>2+</sup> ions with two neighboring framework Al in 6-membered rings that provide two negative framework charges (Z2Cu); and (2) [Cu(OH)]<sup>+</sup> with one framework Al in the 8-membered rings needed one negative framework charge (ZCuOH). Subsequently, the effect of sulfur on Z2Cu and ZCuOH sites was studied in-depth [36,49], and the results show that the extent to which these two Cu species are poisoned by sulfur are extremely different. ZCuOH more readily interacts with SO<sub>2</sub> than Z2Cu does, and this interaction leads to the formation of highly stable sulfur species. This hypothesis is further supported by theoretical first-principle simulations [39].

Overall, previous studies have systematically explored the effects of sulfur poisoning on state-of-the-art Cu/CHA catalysts (i.e., Cu/SSZ-13 and Cu/SAPO-34) and have demonstrated the sulfur sensitivity of these small-pore molecular sieves. Nonetheless, little attention has been paid to the impact of sulfur on Cu/LTA catalysts mainly because Cu/LTA as a SCR catalyst is currently fairly novel. To the best of our knowledge, only the study by Ryu et al. [34] mentions SO<sub>2</sub> poisoning of Cu/LTA catalysts, and that study only conducted one simple SO<sub>2</sub> (20 ppm) exposure effect on NH<sub>3</sub>-SCR activity without any further characterization studies. Thus, the influence of sulfur poisoning on the active sites and the poisoning mechanisms of Cu/LTA, which is a potential next generation SCR catalyst, have still not been studied.

The present study compares the newly emerged Cu/LTA catalyst with the state-of-the-art Cu/SSZ-13 catalyst. Two model samples with analogous chemical components, i.e., Cu/LTA and Cu/SSZ-13 (Si/Al ~ 15, Cu/Al ~ 0.45), were prepared for sulfur poisoning and regeneration investigations. The fresh and sulfated materials were further characterized with a number of spectroscopic methods, including H<sub>2</sub>-TPR, *in-situ* DRIFTS, various SO<sub>2</sub>-TPD and NH<sub>3</sub>-TPD, in order to elucidate the catalyst structure/function relationships and to attain insight into the catalytic deactivation mechanism upon sulfur poisoning.

## 2. Experimental section

### 2.1. Catalyst synthesis

Both Na/SSZ-13 (Si/Al ~ 15) and H/LTA (Si/Al ~ 15) were hydrothermally synthesized in-house using methods previously reported [35,50,51]. After synthesis, separation, drying, and calcination, the obtained Na/SSZ-13 was ion-exchanged with a 5.4 M NH<sub>4</sub>NO<sub>3</sub> solution twice for 1 h at 80 °C to obtain NH<sub>4</sub>/SSZ-13. Then the NH<sub>4</sub>/SSZ-13 was calcined again to obtain H/SSZ-13. Cu/zeolites (i.e., SSZ-13 and LTA) were prepared using the incipient wetness impregnation (IWI) method. The details can be found in our prior publication [35]. Briefly, a certain amount of Cu(NO<sub>3</sub>)<sub>2</sub>·2.5H<sub>2</sub>O was added to ethanol while stirring until completely dissolved. Then the zeolite (H/LTA or H/SSZ-13) was slowly introduced into the solution, and the mixture vessel was capped and stirred for 15 min. After this, the product was dried at room temperature overnight in a fume hood.

The as-prepared powder was fully ground before calcination at 600 °C for 8 h, then ramped up to 750 °C for 2 h in static air. The obtained powder was used to coat a monolith (400 cpsi) that was 15 mm in diameter and 20 mm in length. The details of the washcoat procedure can be found in our prior work [52]. Alumina (Disperal P2, Sasol) was used as a binder when coating the zeolite to increase the attachment of the zeolite, with a ratio of around 95/5 between the zeolite and binder. The total washcoat weight was ~300 mg, including the binder. The prepared monolith was then calcined at 500 °C for 2 h. Prior to use, the monolith was first degreased at 750 °C for 4 h under standard SCR reaction conditions (400 ppm NO, 400 ppm NH<sub>3</sub>, 5% H<sub>2</sub>O, 10% O<sub>2</sub>, 1200 ml/min) in a flow reactor (described in Section 2.3). This step can further facilitate the movement of copper species into ion-exchanged positions, and indeed we observed that the color of the samples changed from grayish blue to pure blue.

### 2.2. Catalyst characterization

The Cu, Si, and Al contents of the samples were measured with Inductively Coupled Plasma Atomic Emission Spectroscopy (ICP-AES) conducted by ALS Scandinavia AB.

H<sub>2</sub> temperature-programmed reduction (H<sub>2</sub>-TPR) of the samples was performed on a Differential Scanning Calorimeter (Sensys DSC, Setaram) connected to a mass spectrometer (Hiden HPR-20 QUI MS) to detect outlet gases. Measurements were conducted on both fresh and sulfated samples (i.e., Cu/LTA and Cu/SSZ-13). Sulfated samples were first exposed to SO<sub>2</sub> (400 ppm NO, 400 ppm NH<sub>3</sub>, 30 ppm SO<sub>2</sub>, 10% O<sub>2</sub>, 5% H<sub>2</sub>O, and balance Ar) at 250 °C for 2 h in a flow reactor (see Section 2.3). TPR was conducted from room temperature to 800 °C at 10 °C/min in 2000 ppm H<sub>2</sub> balanced with Ar. Note that no pretreatment was performed on the samples prior to the TPR experiments.

*In-situ* Diffuse Reflectance Infrared Fourier Transform Spectra (DRIFTS) were acquired with a Bruker Vertex 70 spectrometer, equipped with an MCT detector and operated at 4 cm<sup>-1</sup> resolution. Each spectrum reported was obtained by averaging 256 scans. Prior to each measurement, the catalysts were pretreated by heating in 100 ml/min 10% O<sub>2</sub>/Ar to 500 °C and maintained at this temperature for 1 h. The ZCuOH and Z2Cu species were studied through framework internal asymmetric T-O-T vibrations [53]. This was done by cooling the catalysts to 200 °C to carry out the adsorption of NH<sub>3</sub> (300 ppm NH<sub>3</sub>, 10% O<sub>2</sub>, balance Ar) until saturation. Subsequently, the catalyst was purged in 10% O<sub>2</sub>/Ar for 20 min, which was followed by NO exposure (300 ppm NO, 10% O<sub>2</sub>, balance Ar) for 3 h. The spectra were recorded as a function of time using the background measured at 200 °C in a flow of 10% O<sub>2</sub>/Ar, prior to the introduction of NH<sub>3</sub>. To study SO<sub>2</sub> poisoning, the catalysts were first exposed to SO<sub>2</sub> (30 ppm SO<sub>2</sub>, 10% O<sub>2</sub>, balance Ar) at 200 °C for 2 h and spectra were taken.

NH<sub>3</sub> temperature-programmed desorption (NH<sub>3</sub>-TPD) was carried out using a flow reactor system with NH<sub>3</sub> detection via an online MKS

2030 FTIR analyzer (see Section 2.3). The same monoliths (~300 mg catalyst) used for the SCR reactions (see Section 2.3) were used for the  $\text{NH}_3$ -TPD measurements, and the experimental steps were as follows: (1) heat the sample to 500 °C in 10%  $\text{O}_2$ /Ar (1200 ml/min) and keep at 500 °C for 20 min; (2) cool the sample to  $\text{NH}_3$  adsorption temperatures of 100 °C in 10%  $\text{O}_2$ /Ar; (3) adsorb  $\text{NH}_3$  (400 ppm  $\text{NH}_3$ , 10%  $\text{O}_2$ , 5%  $\text{H}_2\text{O}$ , 30 ppm  $\text{SO}_2$  (if needed)) in Ar until the outlet  $\text{NH}_3$  concentrations remained constant for 1 h; (4) flush the catalyst with 10%  $\text{O}_2$  in Ar, and 5%  $\text{H}_2\text{O}$ , 30 ppm  $\text{SO}_2$  (if needed); (5) then purge with Ar for 20 min at the adsorption temperature (i.e., 100 °C); and (6) ramp from the adsorption temperature to 750 °C at 20 °C/min, and maintaining the temperature at 750 °C for 20 min.

$\text{SO}_2$  temperature-programmed desorption ( $\text{SO}_2$ -TPD) was performed using the same procedure as described above for  $\text{NH}_3$ -TPD. A new monolith was used for each sulfur TPD experiment with the same batch of Cu/LTA and Cu/SSZ-13. Briefly, the experimental steps were as follows: (1) heat the monolith sample to 500 °C in 10%  $\text{O}_2$ /Ar (1200 ml/min) and keep at 500 °C for 20 min; (2) cool the sample to the  $\text{SO}_2$  adsorption temperature of 250 °C in 10%  $\text{O}_2$ /Ar; (3) adsorb  $\text{SO}_2$  (30 ppm  $\text{SO}_2$ , 10%  $\text{O}_2$  in Ar, 5%  $\text{H}_2\text{O}$  (if needed), 400 ppm  $\text{NH}_3$  (if needed)) until outlet  $\text{SO}_2$  concentrations remained constant for 2 h; (4) turn off the  $\text{SO}_2$  flow, and flush with 5%  $\text{H}_2\text{O}$  (if needed), 400 ppm  $\text{NH}_3$  (if needed) and 10%  $\text{O}_2$ ; (5) then purge with Ar for 20 min at the adsorption temperature (i.e., 250 °C); and (6) ramp from the adsorption temperature to 750 °C using a ramp speed of 20 °C/min, and maintain the temperature at 750 °C for 20 min.

### 2.3. Reaction tests

$\text{NH}_3$ -SCR reactions were conducted on washcoated monoliths in a flow reactor. Details about the reactor system can be found in our previous publication [52]. Briefly, the gases were mixed using several Bronkhorst MFCs, and the water was added with a Bronkhorst CEM system. Concentrations of reactants and products were measured with an online MKS 2030 FTIR analyzer. For a standard SCR reaction ( $4\text{NO} + 4\text{NH}_3 + \text{O}_2 \rightarrow 4\text{N}_2 + 6\text{H}_2\text{O}$ ), the feed gas contained 400 ppm NO, 400 ppm  $\text{NH}_3$ , 10%  $\text{O}_2$ , 5%  $\text{H}_2\text{O}$  with Ar as the inert balance. For a fast SCR reaction ( $\text{NO} + \text{NO}_2 + 2\text{NH}_3 \rightarrow 2\text{N}_2 + 3\text{H}_2\text{O}$ ), 400 ppm NO was replaced with 200 ppm NO and 200 ppm  $\text{NO}_2$ . The other feed was the same as for a standard SCR reaction. Measurements were conducted from high to low reaction temperatures, and monoliths were maintained at each target temperature for 30 min. Note that steady state was not attained at 150 °C, and the last point was shown for the conversion. All the gas lines were maintained above 100 °C to avoid water condensation. The total gas flow was 1200 sccm, and the gas hourly space velocity (GHSV) was estimated to be  $22100 \text{ h}^{-1}$  for the monolith (with a washcoat amount of ~300 mg).

Both standard SCR and fast SCR reactions were conducted on fresh, sulfated, and different temperature-regenerated (i.e., 400, 500, 600, and 750 °C) samples. First, the catalyst was degreened using 5%  $\text{H}_2\text{O}$ , 10%  $\text{O}_2$  in Ar at 750 °C for 4 h. Thereafter, the activity was measured for standard SCR and fast SCR reactions. For the fresh catalyst a pre-treatment was done prior to each experiment (500 °C for 20 min using 5%  $\text{H}_2\text{O}$ , 10%  $\text{O}_2$  in Ar). Note that no pre-treatment was done after poisoning. Thereafter, the temperature was set to 250 °C and maintained at this temperature for 0.5 h under standard SCR conditions (400 ppm NO, 400 ppm  $\text{NH}_3$ , 10%  $\text{O}_2$ , 5%  $\text{H}_2\text{O}$  and balance Ar). This was followed by adding 30 ppm  $\text{SO}_2$  to the feed gas for 2 h, followed by a purge in the SCR gas phase again for 0.5 h ( $\text{SO}_2$  was turned off). After this, the sulfate samples were continuously regenerated at 400, 500, 600, and 750 °C with standard and fast SCR tests between each regeneration temperature.

## 3. Results and discussion

In this work, we compared two types of Cu/zeolites, Cu/LTA and

**Table 1**

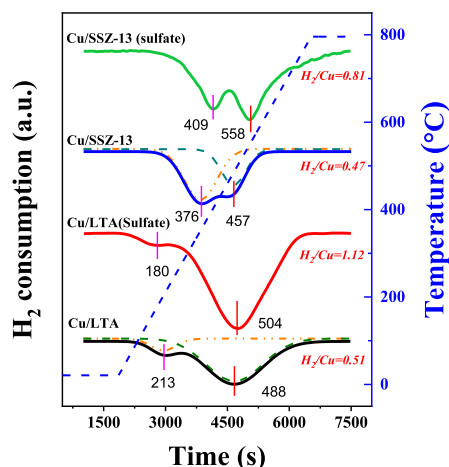
ICP-AES results for the Cu/LTA and Cu/SSZ-13 samples.

sample	Si content (wt.%)	Al content (wt.%)	Cu content (wt.%)	Si/Al ratio	Cu/Al ratio
Cu/LTA	38.9	2.6	2.9	14.4	0.47
Cu/SSZ-13	37.8	2.4	2.5	15.2	0.44

Cu/SSZ-13, with analogous chemical compositions. As shown in Table 1, the Si/Al ratios of Cu/LTA and Cu/SSZ-13 were 14.4 and 15.2, respectively, and the corresponding Cu/Al ratios were 0.47 and 0.44. Note that, in this study, an Si/Al ratio close to 15 of the zeolites was selected since this ratio is close to the commercial catalysts applied in the EATS of diesel vehicles [53,54]. A Cu/Al ratio close to but less than 0.5 was preferred for Cu loading (e.g., 0.47 for Cu/LTA). This not only avoids the formation of abundant  $\text{CuO}_x$  clusters but also achieves the utmost catalytic activity [34,48].

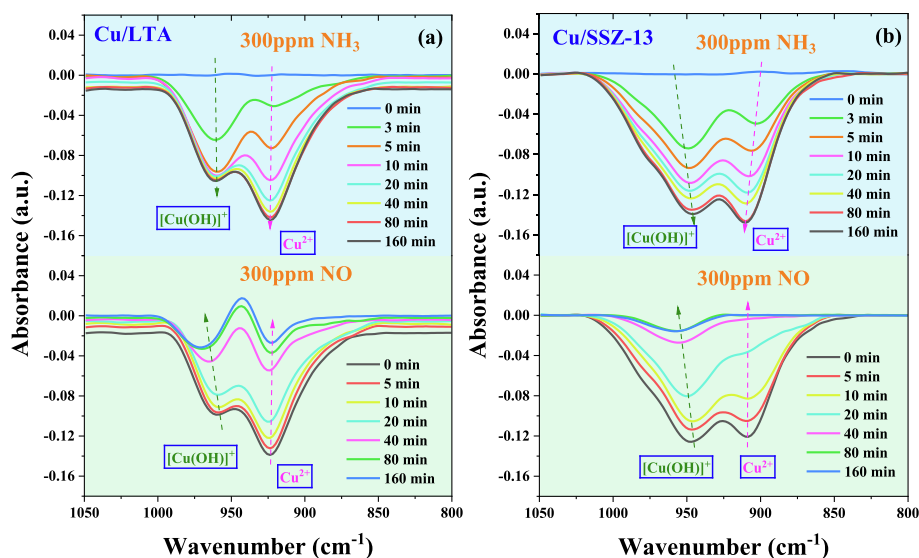
### 3.1. $\text{H}_2$ -TPR results

$\text{H}_2$ -TPR was conducted from ambient conditions without any pre-treatment to investigate the reducibility of fresh and sulfated Cu/zeolites. Fig. 1 shows the  $\text{H}_2$ -TPR results for the Cu/LTA and Cu/SSZ-13 samples. First, two distinct reduction peaks were observed in the fresh catalysts from the TPR curves for both Cu/LTA and Cu/SSZ-13, which was expected. It has previously been suggested that the ZCuOH can be anticipated to show a reduction peak at a lower temperature since the binding energy with the framework of ZCuOH is lower than that of Z2Cu [35]. Therefore, the low-temperature reduction peaks at 213 and 376 °C for fresh Cu/LTA and Cu/SSZ-13, respectively, were attributed to  $[\text{Cu}(\text{OH})]^+$  (i.e.,  $\text{ZCuOH} \rightarrow \text{Cu}^+$ ). And the corresponding high-temperature peaks, occurring at 488 and 457 °C, were attributed to the reduction of  $\text{Cu}^{2+}$  (i.e., Z2Cu) to  $\text{Cu}^+$ . Since the reduction of  $\text{Cu}^+$  to  $\text{Cu}^0$  requires the degradation of the zeolite framework, the reaction process typically occurs above 800 °C [55,56]. This exceeded the measurement range of our instrument (25–800 °C), thus, we could not detect the reduction feature in terms of  $\text{Cu}^+ \rightarrow \text{Cu}^0$ . One key feature that we found, however, was a dramatic reduction temperature discrepancy regarding ZCuOH between fresh Cu/LTA and Cu/SSZ-13 samples, i.e., 213 versus 376 °C, which is approximately a 160 °C difference. Meanwhile, Z2Cu was reduced by  $\text{H}_2$  at comparable temperatures (488 and 457 °C). According to the literature, the  $\text{H}_2$ -TPR reduction peaks of ZCuOH and Z2Cu were different in the same type of Cu/zeolite. There are many possible reasons for this, such as Si/Al ratios, Cu loadings, and the TPR conducted conditions (e.g., ramp rate).



**Fig. 1.**  $\text{H}_2$ -TPR curves for the fresh and sulfated Cu/LTA and Cu/SSZ-13 samples.





**Fig. 2.** DRIFTS spectra of T-O-T vibrational region perturbed by  $\text{NH}_3$  adsorption (upper panels) and followed by NO feeding to react with preadsorbed  $\text{NH}_3$  over time (lower panels) for (a) Cu/LTA and (b) Cu/SSZ-13.

However, in this work, we controlled these conditions using similar Si/Al ratios, similar Cu loadings, and the TPR conditions for Cu/LTA and Cu/SSZ-13 samples were identical. Since we observe such a large gap (213 vs 376 °C) for reduction of ZCuOH, we suggest that this should be mainly due to the different ZCuOH binding energy in Cu/LTA compared to Cu/SSZ-13. Therefore, it can be inferred that, in comparison to Cu/SSZ-13, ZCuOH residing in Cu/LTA is likely to have a much lower binding energy to the framework, resulting in a lower reduction temperature.

To obtain the distribution in Z2Cu and ZCuOH of Cu/LTA and Cu/SSZ-13 samples, peak fitting was used to determine the ratios based on the area of these two Cu species for fresh samples. Briefly, in Cu/LTA, the TPR showed 12% of the ZCuOH sites and 88% of the Z2Cu sites. Meanwhile, ZCuOH was shown to be the dominant Cu site in the Cu/SSZ-13 sample, where 65% of the populations were from TPR. This is an interesting finding. Previous studies have shown that Cu/LTA is more resistant to high-temperature hydrothermal aging than Cu/SSZ-13 is [34,35,57]. The conversion of ZCuOH to  $\text{CuO}_x$  is widely believed to be the main cause of high-temperature deactivation in Cu/SSZ-13. We have earlier found an unusual stability of ZCuOH under different harsh aging temperatures up to 900 °C, which might be one of the reasons for the extraordinary hydrothermal stability of the Cu/LTA sample, together with the stability of Brønsted acid sites and the conversion of  $\text{CuO}_x$  to active Cu sites upon aging [35]. In addition, there was also a significantly larger amount of Z2Cu in the Cu/LTA sample, and this could be another reason for the extraordinary stability of Cu/LTA. Another key feature that we propose based on the different concentrations of Cu species, i.e., Z2Cu and ZCuOH, is the difference in Al distribution among these two zeolites. Specifically, it is clear that Z2Cu needs two Al nearby for charge balance, whereas only one Al is needed for ZCuOH. Therefore, the significantly higher content of Z2Cu in the Cu/LTA sample suggests that more of the Al sites in the LTA are located in pairs in the zeolite framework, as is required for Z2Cu formation. However, this was not the case for the Cu/SSZ-13 sample.

The sulfated Cu/LTA and Cu/SSZ-13 samples showed significantly higher  $\text{H}_2$  consumption than the fresh samples, as displayed in Fig. 1. A similar phenomenon has also been found by Wijayanti et al. and Shen et al. [38,43] who studied the  $\text{SO}_2$  poisoning of Cu/SSZ-13 and Cu/SAPO-34 catalysts, respectively. The total  $\text{H}_2$  consumption, i.e., the  $\text{H}_2/\text{Cu}$  ratio, over fresh and sulfated samples was calculated by integrating the peaks from 25 to 800 °C (2000 ppm  $\text{H}_2$  as a feed). The  $\text{H}_2/\text{Cu}$  ratios for the fresh samples were determined to be 0.51 and 0.47 for Cu/LTA

and Cu/SSZ-13, respectively, which is in line with our discussion above that divalent Cu ions, including ZCuOH and Z2Cu, only undergo a reduction of one-electron below 800 °C [36,48,58]. Note that even though the ratio of  $\text{H}_2/\text{Cu}$  in Cu/zeolites is ca 0.5, we cannot rule out the existence of small amounts of  $\text{CuO}_x$ .

The total  $\text{H}_2$  consumption per Cu for the two sulfated Cu/zeolites were different; 1.12 and 0.81 for sulfated Cu/LTA and Cu/SSZ-13 samples, respectively. Thus, in terms of the  $\text{H}_2$  consumption, it can clearly be seen that the Cu/LTA sample was more influenced by  $\text{SO}_2$  poisoning. According to Shen et al and He et al [43,59], the higher  $\text{H}_2$  consumption of the sulfated Cu/zeolites can be attributed to: (1) the reduction of the sulfated Cu species from the divalent to the metallic state, which only requires one single step ( $\text{Cu}^{2+} \rightarrow \text{Cu}^0$ ); and (2) the reaction of  $\text{H}_2$  with sulfate species. Point (2) has been confirmed in earlier studies (MS) [38,43] in which  $\text{H}_2\text{S}$  formation was observed at around 650 °C for  $\text{SO}_2$  poisoned samples using mass spectrometry. This finding was also indirectly demonstrated in the present study by the fact that the  $\text{H}_2/\text{Cu}$  ratio of sulfated Cu/LTA (~1.12) exceeded one, since one copper ion requires, at the most, one  $\text{H}_2$  molecule.

### 3.2. In situ DRIFTS results

Based on the perturbation to asymmetric T-O-T vibrations of the zeolite framework, Z2Cu ions residing close to pair Al sites and ZCuOH ions close to single Al sites can clearly be distinguished in Cu/zeolites (e.g., SSZ-13 or LTA), especially with the help of  $\text{NH}_3$  [31,33,49]. Therefore, to further investigate the effect of these two types of zeolite structure on the distribution of Cu species and the impact on SCR reactions, in situ DRIFTS of  $\text{NH}_3$  adsorption followed by NO feeding over time were conducted. The results are shown in Fig. 2a and b, for Cu/LTA and Cu/SSZ-13, respectively. Prior to measurements, the samples were dehydrated in 10%  $\text{O}_2/\text{Ar}$  for 1 h at 500 °C to exclude perturbation from  $\text{H}_2\text{O}$ . Backgrounds were measured at 200 °C in a flow of 10%  $\text{O}_2/\text{Ar}$ .

Two well-resolved negative bands were clearly observed for both Cu/LTA and Cu/SSZ-13 samples. Compared with Cu/SSZ-13, Cu/LTA exhibited a shift in the IR signals to higher wavenumbers, which has been observed previously [35,60]. Specifically, as we can see from Fig. 2a and b, features at approximately 925 and 960  $\text{cm}^{-1}$  were detected for Cu/LTA, while slightly lower signals at 900 and 950  $\text{cm}^{-1}$  were detected for Cu/SSZ-13. These features corresponded to Z2Cu and ZCuOH species, respectively [53,60]. The signal shift is suggested to be

due to the difference in framework structure between LTA and CHA topology. As shown in the upper panels of Fig. 2a and b, the samples were fully saturated within 160 min during the  $\text{NH}_3$  adsorption step. The evolution of these two Cu species over time upon  $\text{NH}_3$  adsorption gives interesting information regarding these two Cu/zeolites. For example,  $\text{NH}_3$  preferentially adsorbed onto the ZCuOH sites of the Cu/LTA sample, i.e.,  $960\text{ cm}^{-1}$  (Fig. 2a), where the signal intensity of ZCuOH sites increased significantly faster than the intensity of the signal of the Z2Cu sites. The ZCuOH sites were saturated after only approximately 5 min. This was perhaps due to the stronger interaction between the ZCuOH sites and  $\text{NH}_3$  molecules than between the Z2Cu sites and  $\text{NH}_3$  molecules. Similar to the Cu/LTA sample, ZCuOH was the preferred adsorption site compared to Z2Cu for the Cu/SSZ-13 sample (Fig. 2b), however, this difference disappeared over time. The reason for this is suggested to be that the Cu/SSZ-13 sample used in the study contained a higher concentration of ZCuOH than Z2Cu, as shown in the  $\text{H}_2$ -TPR profiles (Fig. 1).

Following  $\text{NH}_3$  adsorption (300 ppm  $\text{NH}_3$ , 10%  $\text{O}_2$ , balance Ar) and Ar purge for 20 min, NO (300 ppm NO, 10%  $\text{O}_2$ , balance Ar) was added to the feed gas. Fig. 2a and b (lower panels) display the DRIFTS spectra obtained during the reaction between NO and pre-adsorbed  $\text{NH}_3$  with the Z2Cu and ZCuOH sites at  $200^\circ\text{C}$  for Cu/LTA and Cu/SSZ-13, respectively. The adsorbed  $\text{NH}_3$  was consumed gradually over time following the addition of 300 ppm NO to both Cu/zeolites, which was observed by the decrease in the two negative IR features at  $900\text{--}930$  and  $950\text{--}960\text{ cm}^{-1}$  towards baseline [36]. This phenomenon confirms that both the ZCuOH and Z2Cu residing in the zeolites (i.e., LTA and CHA) were active for the  $\text{NH}_3$ -SCR reaction at  $200^\circ\text{C}$  [33,61]. Although the overall trend was identical, a few key differences between the two types of zeolite were, nevertheless, found. First, slight negative bands were observed in both of the Cu/LTA and Cu/SSZ-13 samples after flowing in NO for 160 min. Specifically, solely one weak negative feature located at  $950\text{ cm}^{-1}$  (i.e., ZCuOH) remained in the Cu/SSZ-13 sample, while the band at  $900\text{ cm}^{-1}$  (i.e., Z2Cu) completely returned to baseline. This suggests that all the  $\text{NH}_3$  adsorbed onto Z2Cu can react with NO, yet a very small portion of the  $\text{NH}_3$  adsorbed onto ZCuOH cannot be consumed by NO, or the reaction rate is quite low at  $200^\circ\text{C}$ . Moreover, it is worth noting that both of the negative bands of the Cu/LTA sample at  $960$  and  $925\text{ cm}^{-1}$  partly remained, indicating that not only ZCuOH but also some Z2Cu did not readily function in the  $\text{NH}_3$ -SCR reaction at  $200^\circ\text{C}$  for this sample. Therefore, based on the above results, we concluded that there is always a small amount of ZCuOH that cannot, or only slowly, participates in the SCR reaction, regardless if the sample is Cu/LTA or Cu/SSZ-13. However, some Z2Cu sites were not involved in the SCR reaction at  $200^\circ\text{C}$  in the Cu/LTA sample. This could be due to either: (1) a portion of the Cu species being less active for an ammonia SCR reaction, or (2) the location of some Cu species, resulting in that not all species were accessible for NO after  $\text{NH}_3$  adsorption, possibly due to steric hindrance [62].

To further confirm the distribution of Z2Cu and ZCuOH species for Cu/LTA and Cu/SSZ-13 samples with similar Cu/Al ( $\sim 0.45$ ) and Si/Al ( $\sim 15$ ) ratios, peak fittings were conducted to determine the relative area ratios of these two Cu ion species. The results are shown in Fig. 3 and listed in Table 2 together with the  $\text{H}_2$ -TPR results. Although DRIFTS cannot be used directly to quantify species, the results strongly support the  $\text{H}_2$ -TPR results (Fig. 1). It was also found that the concentration of ZCuOH in the Cu/SSZ-13 sample was significantly higher than the concentration in the Cu/LTA sample. Specifically, the ratio of Z2Cu to ZCuOH (i.e. the fraction of Z2Cu divided by the ZCuOH based on the  $\text{H}_2$  TPR) was 7.3 (0.88/0.12) for the Cu/LTA sample, but only 0.54 (0.35/0.65) for the Cu/SSZ-13 sample. Note that the samples used in this study was pretreated at  $750^\circ\text{C}$  for 4 h under standard SCR reaction conditions (400 ppm NO, 400 ppm  $\text{NH}_3$ , 5%  $\text{H}_2\text{O}$ , 10%  $\text{O}_2$ , 1200 ml/min) in the flow reactor. Therefore, it is expected that the content of ZCuOH will be higher in fresh Cu/SSZ-13 according to work from Gao et al. [33]. However, based on our previous work [35], the number of

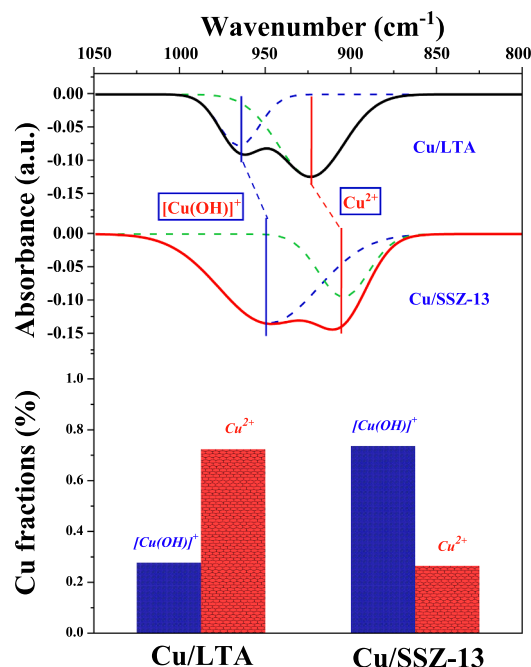


Fig. 3. Comparison of saturated DRIFTS spectra of T-O-T vibrational region perturbed by  $\text{NH}_3$  adsorption for Cu/LTA and Cu/SSZ-13 samples with ZCuOH and Z2Cu populations.

Table 2

The fraction of different Cu species from DRIFTS and  $\text{H}_2$ -TPR for Cu/LTA and Cu/SSZ-13 samples.

Sample		ZCuOH	Z2Cu
Cu/LTA	DRIFTS	0.28	0.72
	$\text{H}_2$ -TPR	0.12	0.88
Cu/SSZ-13	DRIFTS	0.73	0.27
	$\text{H}_2$ -TPR	0.65	0.35

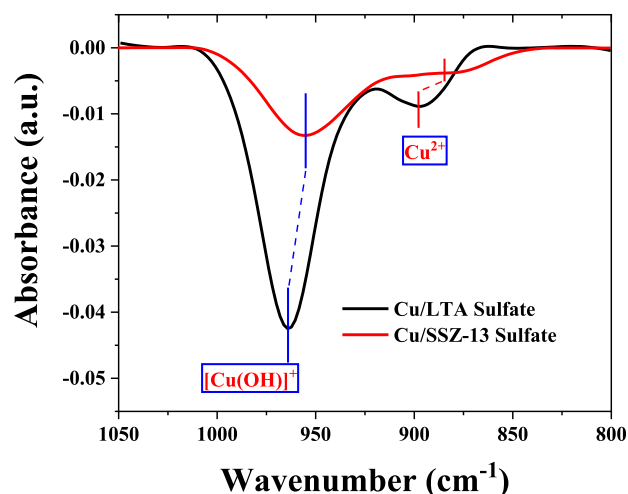


Fig. 4. DRIFTS spectra of T-O-T vibrational region perturbed by  $\text{SO}_2$  poisoning for Cu/LTA (upper panel) and Cu/SSZ-13 (lower panel) samples.

ZCuOH in fresh Cu/LTA will be even lower, as we observed the gradual conversions of both Z2Cu and  $\text{CuO}_x$  clusters to ZCuOH with increasing aging temperature.

Fig. 4 presents the corresponding internal asymmetric T-O-T vibrations for the sulfated Cu/LTA and Cu/SSZ-13 samples (30 ppm  $\text{SO}_2$ ,

10% O<sub>2</sub>, balance Ar at 200 °C for 2 h) using the conditions prior to sulfation as background. Similar to the NH<sub>3</sub> pre-adsorption discussed above, the negative T–O–T vibration features mainly arose from perturbations induced by SO<sub>2</sub> interaction with isolated Cu ions residing close to the framework [36,59], i.e., ZCuOH and Z2Cu. Not surprisingly, two negative features were found at approximately 900–925 and 950–960 cm<sup>−1</sup>, representing Z2Cu and ZCuOH for both Cu/zeolites. This indicates that SO<sub>2</sub> not only can interact with ZCuOH, as suggested in previous research [37,42,63], but can also interact somewhat with Z2Cu sites. However, it should be noted that interaction with Z2Cu sites was minor for both Cu/zeolites. Interestingly, Fig. 4 clearly shows that there was a significantly larger amount of sulfur adsorption onto the ion-exchanged Cu sites inside the Cu/LTA sample than inside the Cu/SSZ-13, especially at the ZCuOH sites. This was somewhat unexpected. As discussed above (Fig. 1 and Fig. 3), ZCuOH was the dominant Cu species in the Cu/SSZ-13 sample, while the majority of the copper in the Cu/LTA catalyst was Z2Cu. Considering that ZCuOH is commonly known to be more reactive with SO<sub>2</sub> [36,39,64], we would expect that the Cu/SSZ-13 sample would more readily interact with SO<sub>2</sub>. However, this was not the case. It was found that ZCuOH sites in the Cu/LTA sample can adsorb more SO<sub>2</sub> despite the lower concentration. The results of the H<sub>2</sub>-TPR method discussed earlier (Fig. 1) can reasonably explain this phenomenon. Since the ZCuOH in the Cu/LTA sample had a weaker interaction with the framework, as indicated by the lower reduction temperature, this makes Cu/LTA more susceptible to SO<sub>2</sub> poisoning than Cu/SSZ-13.

In addition, DRIFTS was also applied to examine the OH vibrational signals in the IR region at 3500–3800 cm<sup>−1</sup> of the Cu/LTA and Cu/SSZ-13 samples after SO<sub>2</sub> poisoning. Fig. 5 depicts the sulfated samples with well-resolved negative/positive bands by using the clean catalyst surface as the background. After SO<sub>2</sub> poisoning, the Cu/LTA and Cu/SSZ-13 samples showed consistent features, i.e., 3734/3735, 3708/3715, 3678/3683, 3650/3654, 3608/3612, and 3564/3582 cm<sup>−1</sup>. The 3734/3735 cm<sup>−1</sup> and 3708/3715 cm<sup>−1</sup> bands can be attributed to the impact of sulfur on isolated and vicinal Si–OH sites, respectively, and the 3678/3683 cm<sup>−1</sup> bands can be attributed to external Al–OH sites. The bands at 3564 and 3612 cm<sup>−1</sup> in the Cu/LTA sample are assigned to Brønsted

acid sites, i.e., Al–OH–Si, where the corresponding bands were 3582 and 3608 cm<sup>−1</sup> for the Cu/SSZ-13 sample. Note here although our Cu/Al ratios were near saturation, i.e., close to 0.5, as shown in Table 1 for the two samples, the intensity of the Brønsted acid sites remained strong. This again confirms the presence of monovalent copper complexes, i.e., ZCuOH, with only one framework Al needed for a charge balance. The reason is that if all the Cu was in the form of Z2Cu, each Cu would need two framework Al, which would consume all the Brønsted acid sites. Since we observe Brønsted acid sites remaining, not all Cu can be in Z2Cu form, thus ZCuOH are also present. Moreover, the bands at 3650/3654 cm<sup>−1</sup> can most likely be attributed to the Cu–OH species [33]. First of all, it is worth mentioning that regardless of whether a peak is positive or negative, it is caused by the effect of SO<sub>2</sub> interaction, since only SO<sub>2</sub> and O<sub>2</sub> are present. Therefore, our results show that in Cu/SSZ-13, only Brønsted acid sites (i.e., Al–OH–Si), Cu–OH and Si–OH were able to interact with SO<sub>2</sub>. However, the interactions of sulfur with the framework were found to be weak for the Cu/SSZ-13 sample.

Interestingly, a large amount of –OH groups in the Cu/LTA sample were found to be significantly affected by SO<sub>2</sub>. Especially, in the case of 3650/3654 cm<sup>−1</sup>, corresponding to Cu–OH sites, the intensity of the Cu/LTA sample was much stronger than that of Cu/SSZ-13. This is in line with the results displayed in Fig. 4. Once again, this confirms that the ZCuOH in the Cu/LTA sample was more susceptible to SO<sub>2</sub> poisoning. Moreover, the intensity of Brønsted acid sites in Cu/LTA catalyst (i.e., 3564 cm<sup>−1</sup>) was stronger than that of Cu/SSZ-13 catalyst (i.e., 3608 cm<sup>−1</sup>) from Fig. 5. This was most likely due to the stronger interaction between Al–OH–Si and SO<sub>2</sub> in Cu/LTA.

### 3.3. SO<sub>2</sub> temperature-programmed desorption (SO<sub>2</sub>-TPD) results

Cu/LTA and Cu/SSZ-13 samples were treated with SO<sub>2</sub> at 250 °C for sulfur deposition under three conditions (i.e., SO<sub>2</sub>, SO<sub>2</sub> + H<sub>2</sub>O, and SO<sub>2</sub> + NH<sub>3</sub> + H<sub>2</sub>O) to gain insight into differences in the SO<sub>2</sub> poisoning of Cu/LTA and Cu/SSZ-13 samples and to understand the influence of the addition of NH<sub>3</sub> and H<sub>2</sub>O. The TPD results are shown in Fig. 6. The SO<sub>2</sub> desorption signals of the Cu/zeolites were integrated to quantify the extent of sulfation under different SO<sub>2</sub> poisoning conditions, shown as mmol/g<sub>washcoat</sub>. The values are presented with inserts in the upper-left corners of the figures and are listed in Table 3.

Only one high-temperature desorption state (> 600 °C) was found for the Cu/LTA and Cu/SSZ-13 samples under dry conditions with only SO<sub>2</sub> present, which was due to the decomposition of copper sulfate species [36,46,65], see Fig. 6 (orange line). Note that the S<sub>High</sub>/ZCuOH ratios have also been calculated and are listed in Table 3, where S<sub>High</sub> represents the amount of SO<sub>2</sub> desorption at high temperature (> 600 °C), and the value of ZCuOH was obtained based on the ICP (Table 1) and H<sub>2</sub>-TPR results (Fig. 1). As confirmed by DRIFTS data (Fig. 4), ZCuOH is significantly more vulnerable to SO<sub>2</sub> than Z2Cu. Thus, using the S<sub>High</sub>/ZCuOH ratio is reasonable since the majority of the formed copper sulfate should be from ZCuOH. The ratio of S<sub>High</sub>/ZCuOH derived from the Cu/LTA sample (0.64) in the presence of SO<sub>2</sub> only is a factor of 10 times larger than the ratio in the Cu/SSZ-13 sample (0.06). This result is consistent with the DRIFTS data (Fig. 4 and Fig. 5) and H<sub>2</sub>-TPR results (Fig. 1), where the ZCuOH sites residing in the Cu/LTA sample were found to be more susceptible to SO<sub>2</sub> due to weaker binding energy with the framework.

One key feature found for both Cu/zeolites was that H<sub>2</sub>O greatly enhances the formation of stable sulfur species (copper sulfate), as shown in the TPD curves (green line), which decompose at high temperature, i.e., above 600 °C. This finding is consistent with the work by Wijayanti et al. [46]. It should be noted that some H<sub>2</sub>SO<sub>4</sub> can be formed in the presence of H<sub>2</sub>O, which is difficult to detect in our reactor system. However, this is only a small amount (ca 10%) based on our adsorption and desorption mass balance calculations and will not affect the trend. Therefore, here, the TPD results suggest that in the presence of H<sub>2</sub>O, ZCuOH is interacting with H<sub>2</sub>O, leading to a dramatic increase in SO<sub>2</sub>

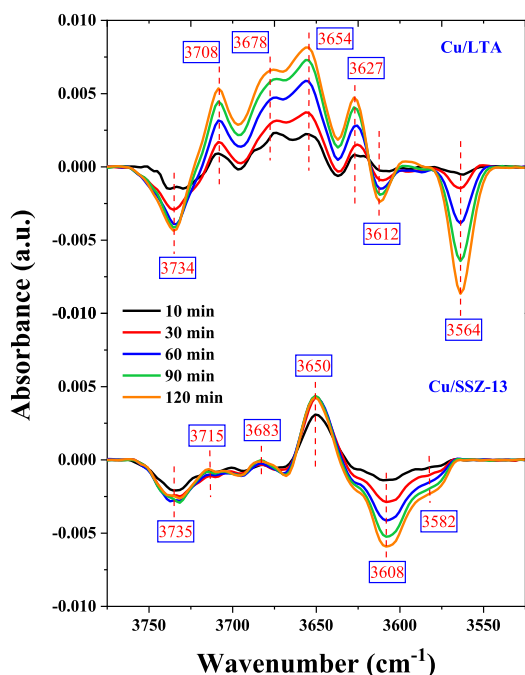
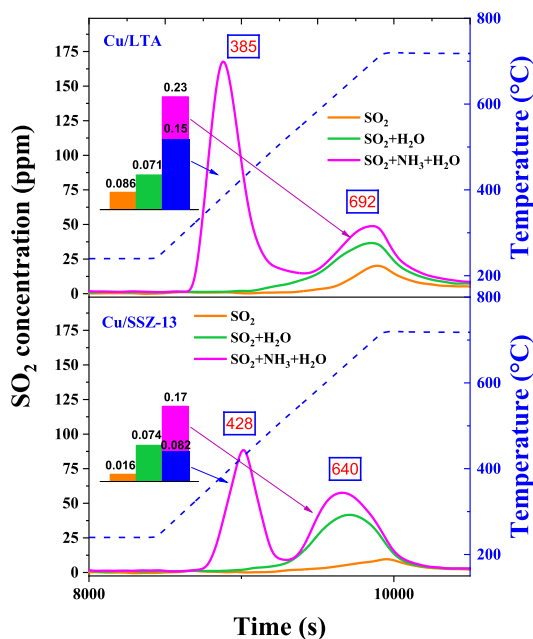


Fig. 5. DRIFTS spectra of the OH vibrational region caused by SO<sub>2</sub> poisoning of the Cu/LTA and Cu/SSZ-13 samples.



**Fig. 6.** SO<sub>2</sub>-TPD profiles for Cu/LTA (upper panels) and Cu/SSZ-13 (lower panels) samples after adsorption with (1) 30 ppm SO<sub>2</sub>, 10% O<sub>2</sub>, balance with Ar (named as SO<sub>2</sub>); (2) 30 ppm SO<sub>2</sub>, 5% H<sub>2</sub>O, 10% O<sub>2</sub>, balanced with Ar (named as SO<sub>2</sub> + H<sub>2</sub>O); (3) 30 ppm SO<sub>2</sub>, 5% H<sub>2</sub>O, 400 ppm NH<sub>3</sub>, 10% O<sub>2</sub>, balanced with Ar (named as SO<sub>2</sub> + NH<sub>3</sub> + H<sub>2</sub>O).

storage for both Cu/zeolites. In this case, the  $S_{\text{High}}/\text{ZCuOH}$  ratio of Cu/LTA is ca 1.31, which is even higher than 1. This should indicate that almost all of the ZCuOH in the Cu/LTA sample was poisoned by sulfur in the presence of H<sub>2</sub>O. The part (~0.31) exceeding 1 may be due to some contribution from Z2Cu sites, as seen in the SO<sub>2</sub> DRIFTS experiments (Fig. 4). However, the ratio of  $S_{\text{High}}/\text{ZCuOH}$  in the Cu/SSZ-13 sample was only ~0.29, suggesting that many ZCuOH sites were not poisoned by sulfur in the presence of H<sub>2</sub>O.

Next, NH<sub>3</sub> was added to the gas phase together with SO<sub>2</sub> and H<sub>2</sub>O, as shown in Fig. 6 (pink line). Compared with the desorption curves of SO<sub>2</sub> only with/without H<sub>2</sub>O, a new SO<sub>2</sub> desorption feature was observed at approximately 385 °C for the Cu/LTA sample and at 428 °C for the Cu/SSZ-13. This new feature is typically attributed to the decomposition of ammonium sulfate ((NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>) species [36,42]. Specifically, for the Cu/LTA sample, ~0.15 mmol/g<sub>washcoat</sub> was from ammonium sulfates, and the corresponding value for the Cu/SSZ-13 sample was ~0.06 mmol/g<sub>washcoat</sub>. Significantly more ammonium sulfates were formed in the Cu/LTA sample. It is known that the cage size of the LTA structure (12.3 Å × 12.3 Å × 12.3 Å) is significantly larger than that of CHA structure (10.9 Å × 6.7 Å × 9.4 Å) [57]. This may also contribute to the formation of more ammonium sulfates in Cu/LTA. The presence of NH<sub>3</sub> can promote the formation of copper sulfate species to a certain

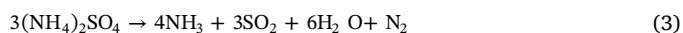
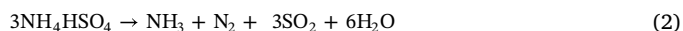
extent since some of the ammonium sulfates can be transformed into copper sulfates during the TPD ramp [46].

### 3.4. NH<sub>3</sub> temperature-programmed desorption (NH<sub>3</sub>-TPD) results

Brønsted and Lewis acid sites were investigated using NH<sub>3</sub>-TPD experiments. The formation and decomposition of ammonium sulfate were further studied using NH<sub>3</sub>/SO<sub>2</sub>-TPD experiments. NH<sub>3</sub> desorption results are presented in Fig. 7a and b (upper panels) for the Cu/LTA and Cu/SSZ-13 samples, respectively, for two NH<sub>3</sub> adsorption conditions, i.e., NH<sub>3</sub> + H<sub>2</sub>O and NH<sub>3</sub> + SO<sub>2</sub> + H<sub>2</sub>O. Two main NH<sub>3</sub> desorption states were found for both Cu/LTA and Cu/SSZ-13 samples without SO<sub>2</sub> during adsorption (black line in the upper panels of Fig. 7): a low-temperature feature at ~200 °C, and a high-temperature feature at ~300 °C. According to previous studies [53,66], the peak at 200 °C is mainly attributed to the desorption of NH<sub>3</sub> from ion-exchanged Cu sites. The high-temperature peak (i.e., 300 °C) is attributed to the desorption of NH<sub>3</sub> from Brønsted acid sites and also partly to the contribution from NH<sub>3</sub> stored on strong Lewis acid sites, i.e., ion-exchanged Cu sites [35]. Interestingly, the capacities for NH<sub>3</sub> storage were greatly improved through all temperature regions in the presence of SO<sub>2</sub> in the adsorption feed gas (red line in the upper panels of Fig. 7).

The increase in NH<sub>3</sub> storage can be attributed to: (1) the newly generated acidic sites, and/or (2) the decomposition of produced ammonium sulfates. New acidic sites occur because some of the anchoring S atoms can be associated with the more acidic hydroxyl group in the form of S-OH, which facilitates a relatively strong coordination binding between the NH<sub>3</sub> molecule and such acidic sites. A similar phenomenon has also been found in phosphorus-poisoned Cu/SSZ-13 samples [11]. Therefore, the subtracted curves (i.e., the TPD curve with SO<sub>2</sub> (red line) minus that without SO<sub>2</sub> (black line)) are also presented in Fig. 7a and b (lower panels) for a more intuitive and clear understanding of the changes to the desorption of NH<sub>3</sub> after the addition of SO<sub>2</sub>. Peak fittings were used to quantify the amount of newly generated NH<sub>3</sub> desorption states after the addition of SO<sub>2</sub> for these two Cu/zeolites. The obtained results are listed in Table 4 together with the amount of desorbed SO<sub>2</sub> that occurred as a result of the decomposition of (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> from SO<sub>2</sub>-TPD (Fig. 6 and Table 3) for comparison. Note that these new features are denoted as T1 (190–210 °C), and T2 (360–390 °C), respectively.

First, it is worth to know that ammonium sulfates ((NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>) decompose upon heating above 250 °C, first forming ammonium bisulfate (NH<sub>4</sub>HSO<sub>4</sub>) and NH<sub>3</sub> (Equation (1)). Subsequently, higher temperatures result in further decomposition to N<sub>2</sub>, NH<sub>3</sub>, SO<sub>2</sub>, and H<sub>2</sub>O (Equation (2)) [67]. The decomposition reaction equations are as follows:

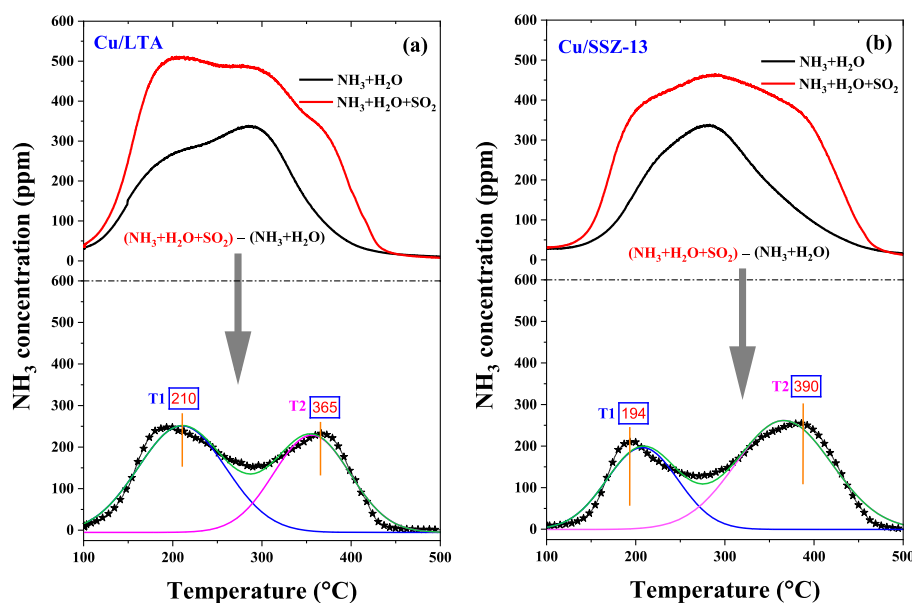


Equation (3) is the overall decomposition process. Since (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> requires at least 250 °C to decompose, then T1 (190–210 °C) should be derived from the newly produced acid sites. T2 can possibly be attributed to the decomposition of (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>, where two steps (Equation (1) and (2)) overlap in the T2 region. Regarding T1, more new acid sites were formed in the Cu/LTA sample than in the Cu/SSZ-13, with the

**Table 3**  
SO<sub>2</sub> storage (mmol/g<sub>washcoat</sub>) and  $S_{\text{High}}/\text{ZCuOH}$  ratios of different adsorption conditions for Cu/LTA and Cu/SSZ-13 samples.

Samples	SO <sub>2</sub>			SO <sub>2</sub> + H <sub>2</sub> O			SO <sub>2</sub> + NH <sub>3</sub> + H <sub>2</sub> O		
	Storage (mmol/g <sub>washcoat</sub> )		$S_{\text{High}}/\text{ZCuOH}$ ratio	Storage (mmol/g <sub>washcoat</sub> )		$S_{\text{High}}/\text{ZCuOH}$ ratio	Storage (mmol/g <sub>washcoat</sub> )		$S_{\text{High}}/\text{ZCuOH}$ ratio
	Low	High		Low	High		Low	High	
Cu/LTA	0	0.035	0.64	0	0.071	1.31	0.15	0.086	1.59
Cu/SSZ-13	0	0.015	0.06	0	0.074	0.29	0.062	0.093	0.37





**Fig. 7.**  $\text{NH}_3$ -TPD profiles for (a) the Cu/LTA sample (upper panel) and (b) the Cu/SSZ-13 sample (upper panel) under two feed conditions (i.e.,  $\text{NH}_3 + \text{H}_2\text{O}$  and  $\text{NH}_3 + \text{SO}_2 + \text{H}_2\text{O}$ ); and the subtracted curves of (a) Cu/LTA (lower panel) and (b) Cu/SSZ-13 (lower panel) from these two condition curves.

**Table 4**

Newly formed  $\text{NH}_3$  storage ( $\text{mmol/g}_{\text{washcoat}}$ ) of two desorption states (i.e., T1 and T2) for the Cu/LTA and Cu/SSZ-13 samples.

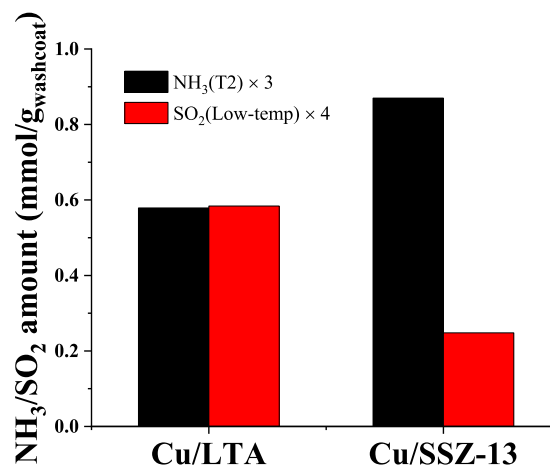
Temperature ( $^{\circ}\text{C}$ )	T1 ( $\text{mmol/g}_{\text{washcoat}}$ )	T2 ( $\text{mmol/g}_{\text{washcoat}}$ )	$\text{SO}_2$ storage (Low-temp) ( $\text{mmol/g}_{\text{washcoat}}$ )
Cu/LTA	0.24	0.19	0.15
Cu/SSZ-13	0.16	0.29	0.062

values of 0.24 and 0.16  $\text{mmol/g}_{\text{washcoat}}$ , respectively.

To confirm our proposal that T2 occurs from the decomposition of ammonium sulfates, and also according to Equation (3), it is clear that the total ratio of generated  $\text{NH}_3$  and  $\text{SO}_2$  upon  $(\text{NH}_4)_2\text{SO}_4$  decomposition is 4 to 3. Therefore, it was interesting to compare the values of  $\text{NH}_3$  storage (T2) from  $\text{NH}_3$ -TPD multiplied by a factor of 3 and  $\text{SO}_2$  storage due to the decomposition of ammonium sulfate from  $\text{SO}_2$ -TPD, multiplied by a factor of 4. The results are calculated and plotted in Fig. 8. Interestingly, the two values were highly identical for the Cu/LTA sample, suggesting that the T2 of Cu/LTA can mainly be attributed to the decomposition of  $(\text{NH}_4)_2\text{SO}_4$ . However, regarding Cu/SSZ-13, the value of ' $\text{NH}_3(\text{T2}) \times 3$ ' was much higher than that of ' $\text{SO}_2$  (Low-temp)  $\times 4$ '. This indicates that the desorption of  $\text{NH}_3$  (T2) from the Cu/SSZ-13 sample cannot only be attributed to the decomposition of ammonium sulfates but also to some  $\text{NH}_3$  desorbed from other sources, such as newly formed acidic sites that are stronger than T1, and/or some  $\text{SO}_2$  that had not desorbed but directly converted to copper sulfate. As discussed in the  $\text{SO}_2$ -TPD section, some of the ammonium sulfate had transformed to copper sulfates during the TPD ramp, however, the amount was limited, with only  $\sim 0.02 \text{ mmol/g}_{\text{washcoat}}$  for the Cu/SSZ-13 sample. Therefore, newly formed strong acidic sites in the T2 region is suggested to be the main explanation. Moreover, a slight delay in the desorption of  $\text{SO}_2$  (Fig. 6) occurred after the decomposition of ammonium sulfate in comparison with the release of  $\text{NH}_3$  (Fig. 7), i.e., the temperatures were 365  $^{\circ}\text{C}$  (390  $^{\circ}\text{C}$ ) with  $\text{NH}_3$  and 385  $^{\circ}\text{C}$  (428  $^{\circ}\text{C}$ ) with  $\text{SO}_2$  desorption for the Cu/LTA (Cu/SSZ-13) samples, respectively.

### 3.5. Reaction results

$\text{SO}_2$  poisoning was conducted under standard SCR reaction



**Fig. 8.** A comparison of  $\text{NH}_3$  storage ( $\text{T2, mmol/g}_{\text{washcoat}} \times 3$ ) and  $\text{SO}_2$  storage from  $(\text{NH}_4)_2\text{SO}_4$  decomposition ( $\text{mmol/g}_{\text{washcoat}} \times 4$ ) for Cu/LTA and Cu/SSZ-13.

conditions. As displayed in Fig. 9, the catalysts were first heated from room temperature to 250  $^{\circ}\text{C}$  and were maintained at this temperature for 0.5 h under standard SCR conditions (400 ppm NO, 400 ppm  $\text{NH}_3$ , 10%  $\text{O}_2$ , 5%  $\text{H}_2\text{O}$  and balance Ar). Thereafter, 30 ppm  $\text{SO}_2$  was doped into the feed gas for 2 h, followed by a purge in the SCR gas again for 0.5 h ( $\text{SO}_2$  was turned off). Cu/zeolites maintained high catalytic activity prior to the addition of  $\text{SO}_2$ . The activity of the sample began to descend immediately after the addition of  $\text{SO}_2$  to the reaction gas. We found that the breakthrough of  $\text{SO}_2$  in the Cu/LTA sample (green line) was slower than in the Cu/SSZ-13 (orange line). This indicates that the Cu/LTA sample was able to store more  $\text{SO}_2$ , which is consistent with the  $\text{SO}_2$ -TPD results. The calculated values of the  $\text{SO}_2$  storage are inserted in Fig. 9, 0.24 and 0.17  $\text{mmol/g}_{\text{washcoat}}$  for the Cu/LTA and Cu/SSZ-13 samples, respectively. This is similar to the amount desorbed from  $\text{SO}_2$ -TPD (0.23 and 0.16  $\text{mmol/g}_{\text{washcoat}}$ ; Fig. 6). It is clear that more than 95% of stored  $\text{SO}_2$  in the catalyst was released and only minor amount (5% or less) of sulfur might remain after the TPD.

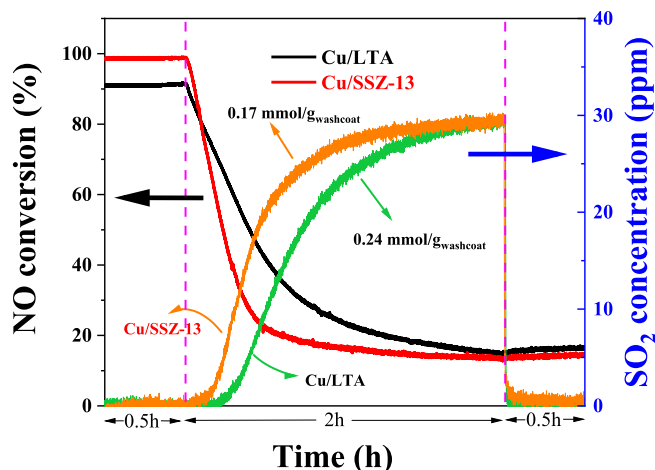


Fig. 9. NO conversions of standard SCR reaction during  $\text{SO}_2$  poisoning at  $250^\circ\text{C}$  for Cu/LTA and Cu/SSZ-13 samples. The reactant feed contained 400 ppm NO, 400 ppm  $\text{NH}_3$ , 30 ppm  $\text{SO}_2$  (if needed), 10%  $\text{O}_2$ , 5%  $\text{H}_2\text{O}$  balanced with Ar at a GHSV of  $22,100\text{ h}^{-1}$ .

Interestingly, it was observed that the rate of decline in the catalytic activity of the two Cu/zeolites was different. The deactivation rate of the Cu/LTA sample was significantly slower than that of the Cu/SSZ-13. This seems to contradict the results above, which show that the Cu/LTA sample can store more  $\text{SO}_2$  than the Cu/SSZ-13, where the Cu/LTA catalyst was expected to be easier to deactivate through  $\text{SO}_2$  poisoning. However, this is not the case here. According to the  $\text{SO}_2$ -TPD results discussed above, under  $\text{SO}_2 + \text{NH}_3 + \text{H}_2\text{O}$  condition, even though the  $S_{\text{High}}/\text{ZCuOH}$  ratio of the Cu/LTA sample (1.59) was much higher than for the Cu/SSZ-13 (0.37), however, the actual values of poisoned ZCuOH sites were basically the same, 0.086 and 0.093 mmol/g<sub>washcoat</sub>, respectively. Therefore, the key factor for deactivation should be the formation of ammonium sulfates, especially where they are located. The  $\text{SO}_2$ -TPD results (Fig. 6) suggest that more ammonium sulfates were formed in the Cu/LTA sample, and according to the DRIFTS data (Fig. 5), it is clear that large amount of  $-\text{OH}$  groups (e.g., external  $\text{Al}-\text{OH}$  sites) in the Cu/LTA sample can interact with  $\text{SO}_2$ , therefore, it is reasonable that more ammonium sulfates would be formed on these  $-\text{OH}$  groups, which would not affect SCR activity significantly. However, fewer framework  $-\text{OH}$  groups in the Cu/SSZ-13 sample were associated with  $\text{SO}_2$ , and more important is that still plenty of ZCuOH sites were not converted to copper sulfate ( $S_{\text{High}}/\text{ZCuOH} \sim 0.37$ ). It is believed that  $(\text{NH}_4)_2\text{SO}_4$  would preferably attach to these unconverted ZCuOH sites, which would seriously affect SCR activity. Thus, the slow deactivation of the Cu/LTA sample is reasonable due to the diversity of the locations of  $(\text{NH}_4)_2\text{SO}_4$ .

Fig. 10(a) and (c) depict the standard  $\text{NH}_3$ -SCR ( $4\text{NH}_3 + 4\text{NO} + \text{O}_2 \rightarrow 4\text{N}_2 + 6\text{H}_2\text{O}$ ) light-off curves of  $\text{NO}_x$  for fresh, sulfated, and regenerated (400, 500, 600, and  $750^\circ\text{C}$ ) Cu/LTA and Cu/SSZ-13 samples, respectively. The  $\text{SO}_2$  poisoning process of the sulfated samples is described in detailed in the previous paragraph. Following this process, the sulfate samples were continuously regenerated at 400, 500, 600, and  $750^\circ\text{C}$  in 10%  $\text{O}_2/\text{Ar}$  for 2 h. Noteworthy, for fresh samples, regardless whether the reactions were standard or fast SCR, Cu/SSZ-13 experienced a more severe selectivity decline than Cu/LTA at high temperature. The  $\text{NO}_x$  conversion of the Cu/SSZ-13 sample was reduced by 40% (from 100% at  $400^\circ\text{C}$  to 60% at  $550^\circ\text{C}$ ) for the fast SCR reaction, which is almost twice the reduction in conversion for the Cu/LTA sample (from 100% at  $400^\circ\text{C}$  to 80% at  $550^\circ\text{C}$ ). As we know, the presence of  $\text{CuO}_x$  clusters in Cu/zeolites is typically claimed to be responsible for the subsequent decline in catalyst selectivity at high reaction temperatures due to ammonia oxidation [33,68].

Another difference between fresh Cu/LTA and Cu/SSZ-13 samples

that deserves attention is the low-temperature catalytic activity for standard and fast SCR reactions. Briefly, the performance of the Cu/SSZ-13 sample was better than the performance of the Cu/LTA in the low-temperature interval for the standard SCR reaction. This is in line with the DRIFTS results shown in Fig. 2, where both Cu active sites are less reactive to  $\text{NO} + \text{NH}_3$  reaction in Cu/LTA as compared to Cu/SSZ-13. However, the performance of these two samples were similar for fast SCR reactions [35,60]. For example, at 175 and  $200^\circ\text{C}$  of standard SCR reaction, the  $\text{NO}_x$  conversions of the Cu/LTA catalyst were 22% and 45%, respectively, while the  $\text{NO}_x$  conversions of the Cu/SSZ-13 were 38% and 71%, respectively. However, in fast SCR reaction, the conversions were 80% and 75% ( $175^\circ\text{C}$ ) for the Cu/LTA and Cu/SSZ-13 samples, respectively, i.e., a fast SCR reaction is less sensitive to the type of Cu species used. There are several possible reasons for this difference in standard SCR reaction, such as: (1) the zeolite framework structure diversity between LTA and CHA; (2) the difference in ZCuOH and Z2Cu population, i.e. ZCuOH and Z2Cu are dominant in Cu/SSZ-13 and Cu/LTA, respectively; (3) the location of some Cu species in the Cu/LTA sample, that are not accessible for NO after the adsorption of  $\text{NH}_3$ , according to the DRIFTS results (Fig. 2). This is possibly due to steric hindrance. Regarding point (1), we examined standard and fast SCR reactions for H/LTA and H/SSZ-13 (not shown). No significant difference was found between H/LTA and H/SSZ-13. Therefore, we can rule out the reason (1).

Regarding  $\text{SO}_2$  poisoning, both of the sulfated Cu/zeolites (red lines in Fig. 10) experienced a certain degree of deactivation, regardless of whether a standard or a fast SCR reaction was used. The loss in the conversion of  $\text{NO}_x$  during standard and fast SCR reactions for the Cu/LTA and Cu/SSZ-13 samples is calculated and displayed in Fig. 11. As shown in the figure, the Cu/LTA sample dropped less in the standard SCR reaction than the Cu/SSZ-13 catalyst, but instead decreased more in the fast SCR reaction. Regarding standard SCR, the reason for this difference may just be as simple as the activity of fresh Cu/LTA is less, then the decline seems less, as the activities of sulfated catalysts are similar. However, the reason for standard SCR does not apply to fast SCR. Here, we propose that ZCuOH may be more active for fast SCR reactions, where ZCuOH in the Cu/LTA sample has been fully poisoned.

As the regeneration temperature increased, the activity of the samples gradually recovered. One interesting phenomenon of the Cu/SSZ-13 sample is that after regeneration at  $600^\circ\text{C}$  (orange lines), its high temperature performance was even better than the fresh sample in both standard and fast SCR reactions. This was not found for the Cu/LTA sample, and we suggest that this is related to the  $\text{CuO}_x$  clusters in the sample. Briefly, as we know,  $\text{CuO}_x$  clusters can also interact with  $\text{SO}_2$  to form copper sulfate species, and the required decomposition temperature is approximately  $650\text{--}700^\circ\text{C}$  [36,42], which we also observed in the  $\text{SO}_2$ -TPD profiles (Fig. 6). Therefore, these copper sulfate species are stable after regeneration at  $600^\circ\text{C}$ , which hinders the non-selective oxidation of  $\text{NH}_3$  by  $\text{CuO}_x$  clusters in the Cu/SSZ-13 sample. However, as our group and Jo et al. [35,57] have suggested, the  $\text{CuO}_x$  clusters in the Cu/LTA sample contribute little to the non-selective oxidation of  $\text{NH}_3$ , thus, it is reasonable that similar phenomena would not be observed. This further confirms the various oxidation properties of the  $\text{CuO}_x$  clusters in these two Cu/zeolites.

Finally, upon regeneration at  $750^\circ\text{C}$ , the Cu/LTA catalyst was restored to its original catalytic activity over the full temperature range ( $150\text{--}550^\circ\text{C}$ ) in both standard and fast SCR reactions. However, low temperature activity was fully recovered in the Cu/SSZ-13 sample, but high temperature activity experienced a certain degree of loss in the two SCR reactions. The results suggest that the physical and chemical properties of the Cu/LTA sample had essentially recovered, whereas some negative changes occurred in the Cu/SSZ-13 sample after regeneration at  $750^\circ\text{C}$ . We must emphasize here that, prior to using fresh Cu/LTA and Cu/SSZ-13, they were degreased at  $750^\circ\text{C}$  for 4 h under the reaction condition (400 ppm NO, 400 ppm  $\text{NH}_3$ , 5%  $\text{H}_2\text{O}$ , 10%  $\text{O}_2$  with Ar). Thus, regeneration at  $750^\circ\text{C}$  for 2 h, especially under dry

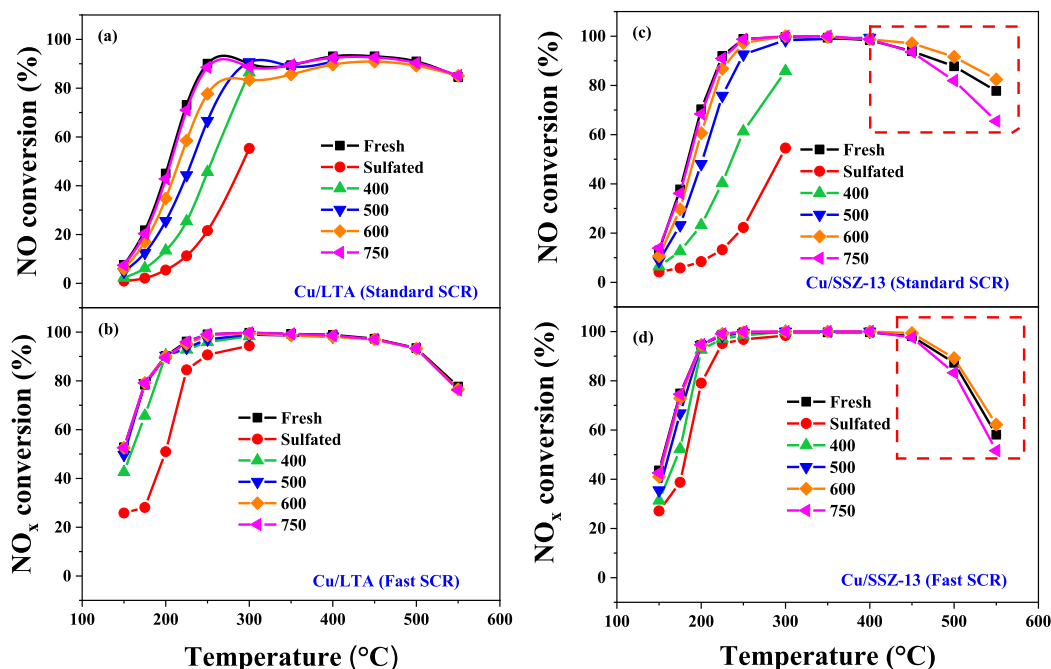


Fig. 10. (a), (c) NO conversion as a function of temperature during standard  $\text{NH}_3$ -SCR, and (b), (d)  $\text{NO}_x$  conversion as a function of temperature during fast  $\text{NH}_3$ -SCR for fresh, sulfated, and different temperature-regenerated (400, 500, 600, and 750 °C) Cu/LTA and Cu/SSZ-13 samples. The reactant feed contained 400 ppm NO (or 200 ppm NO and 200 ppm  $\text{NO}_2$  for fast SCR), 400 ppm  $\text{NH}_3$ , 10%  $\text{O}_2$ , 5%  $\text{H}_2\text{O}$  balanced with Ar at a GHSV of 22,100  $\text{h}^{-1}$ .

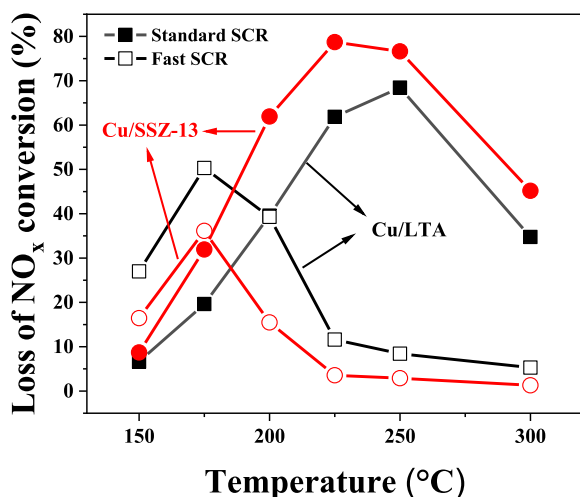


Fig. 11. Loss in conversion of  $\text{NO}_x$  in standard SCR (solid symbols) and fast SCR (hollow symbols) reactions over the Cu/LTA (black lines) and Cu/SSZ-13 (red lines) samples after sulfur poisoning. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

conditions (10%  $\text{O}_2/\text{Ar}$ ), is not supposed to cause any structural degradation of either of the samples, Cu/LTA or Cu/SSZ-13 (Si/Al  $\sim 15$ ). The most likely explanation for the high temperature activity loss of the Cu/SSZ-13 sample is that when copper sulfate species decompose at 750 °C [45,46], a small amount of new  $\text{CuO}_x$  clusters are produced simultaneously as the  $\text{CuO}_x$  clusters in the fresh catalyst are restored. The newly formed  $\text{CuO}_x$  clusters are considered to be the former isolated Cu ions at the ion exchange site, i.e.,  $\text{ZCuOH}$  and/or  $\text{Z}_2\text{Cu}$ , which were detached from the framework during the desulfurization process at 750 °C.

#### 4. Conclusions

Two model catalysts, i.e., Cu/LTA and Cu/SSZ-13, with similar Si/Al and Cu/Al ratios were synthesized using the incipient wetness impregnation (IWI) method. Fresh, sulfated, and different temperature-regenerated (400, 500, 600, and 750 °C) samples were used to study the effect of  $\text{SO}_2$  poisoning and regeneration for standard and fast SCR reactions. A number of characterization methods, including *in-situ* DRIFTS,  $\text{H}_2$ -TPR, various  $\text{NH}_3$ -TPD and  $\text{SO}_2$ -TPD, were used to obtain insight into the catalytic deactivation mechanism upon the sulfur poisoning of Cu/LTA and Cu/SSZ-13 samples.

Both samples contained multiple Cu-containing species, including ion-exchanged  $\text{ZCuOH}$ ,  $\text{Z}_2\text{Cu}$  sites, and a small amount of  $\text{CuO}_x$  clusters. Note that the Cu/SSZ-13 sample contained a higher concentration of  $\text{ZCuOH}$  than the Cu/LTA at similar Cu loadings. This also reflects the difference in the distribution of Al in the two zeolites; more of the Al sites in LTA are located nearby each other. We found that  $\text{SO}_2$  more readily interacts with  $\text{ZCuOH}$  sites than with  $\text{Z}_2\text{Cu}$  sites, which is in line with previous research. However, surprisingly, the  $\text{ZCuOH}$  in the Cu/LTA sample was found to be much more vulnerable to  $\text{SO}_2$  poisoning than the Cu/SSZ-13, due to its lower binding energy with the framework. Moreover,  $\text{SO}_2$ -TPD results show that the presence of  $\text{H}_2\text{O}$  significantly increased sulfur storage.  $\text{NH}_3$ -TPD results suggest that the presence of  $\text{SO}_2$  can contribute to generate new acidic sites that can adsorb  $\text{NH}_3$ , where for Cu/LTA is only at low temperature (T1), but for Cu/SSZ-13, both at low (T1) and high temperature (T2).

Under  $\text{NH}_3$ -SCR reaction conditions in the presence of  $\text{SO}_2$ , the Cu/LTA sample stored much more  $\text{SO}_2$  than the Cu/SSZ-13, and it also had a slower deactivation rate than the Cu/SSZ-13 sample. The additional  $\text{SO}_2$  storage in the Cu/LTA sample was found to be ammonium sulfates, because a large amount of the  $-\text{OH}$  groups in the sample could interact with  $\text{SO}_2$ . Moreover, the  $(\text{NH}_4)_2\text{SO}_4$  in the Cu/SSZ-13 sample is believed to preferably attach to the  $\text{ZCuOH}$  sites that have not transferred to copper sulfate, which results in a faster deactivation rate.

The impact of the  $\text{CuO}_x$  clusters on the Cu/LTA sample on high temperature selectivity was confirmed to be significantly less than the

impact on the Cu/SSZ-13 sample. In addition,  $\text{SO}_2$  poisoning was proved to be able to hinder the non-selective oxidation of  $\text{NH}_3$  by  $\text{CuO}_x$  clusters for Cu/SSZ-13 sample regenerated at 600 °C. Upon regeneration at 750 °C, the Cu/LTA sample could be restored to its original catalytic activity over the full temperature range (150–550 °C) in both standard and fast SCR reactions. However, in terms of Cu/SSZ-13, the low-temperature activity was fully recovered, but high-temperature activity experienced a certain degree of loss in the two SCR reactions. This loss was mainly due to the formation of new  $\text{CuO}_x$  clusters. This further confirms that the Cu/LTA is a robust catalyst with good potential as an SCR catalyst not only towards hydrothermal aging but also towards sulfur poisoning and regeneration.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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