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Special Section:

Radio Channel Modelling
for 5G Millimetre Wave
Communications in Built
Environments

Key Points:

- A semi-analytical model is derived for the Rician K -factor taking into account the impact of the scatterer density and number
- The model is general in the sense that it is not derived for a specific type of scatterers
- A comparison between model and full-wave simulations is in good agreement over a wide frequency span for the considered scatter model

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Semi-Analytical Model of the Rician K -Factor

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Abstract The analysis of the performance of 5G wireless communication systems employing Massive MIMO at millimeter-wave frequencies is of great practical relevance. Of special relevance are the signal fluctuations. In the present paper, we introduce a semi-analytical model for a generic scattering environment by using randomly distributed resonant scatterers to investigate the impact of the size of the scattering environment, the scatterer density, and the number of scatterers on the signal variability in terms of the Rician K -factor as a function of frequency. We further present an investigation of the impact of scattering on the frequency dependence of the signal fading statistics in the 500 MHz–100 GHz band. The simplified model is also verified against full-wave simulation using the Method of Moments (MoM).

1. Introduction

5G wireless communication networks are being developed to meet the increasing demands for better quality-of-service, for example, throughput in the Gbps range. The multiuser multiple-input multiple-output (MU-MIMO) technology employing very large array antennas at the radio base station (RBS), also known as Massive MIMO technology, is one of the key technology enablers (Boccardi et al., 2014). With this technology, the RBS will serve many mobile stations simultaneously, and the data reach each of the mobile antennas by beamforming the energy towards them (Larsson et al., 2014). The combination of large array antennas and many users turns out to be favorable for data transmission. Favorable propagation (FP) conditions mean that the channel vectors between the users and the RBS are nearly pairwise orthogonal. Therefore, the signal processing complexity can be considerably reduced since linear processing is very close to be optimal (Marzetta, 2010; Rusek et al., 2013).

Another enabler is the use of very large portions of the electromagnetic spectrum; that is, in addition to operation in the traditional ultra high frequency (UHF) band, new very large contiguous bandwidths will be exploited at the extremely high frequency (EHF) band, that is, the millimeter-wave (mm-wave) frequencies.

Currently, there is no complete understanding of the propagation characteristics at the frequency bands of interest, that is, from 500 MHz to approximately 100 GHz for Massive MIMO. As is well-known, channel models are indispensable tools for evaluating, predicting, or optimizing the performance of wireless systems (Glazunov, 2014; Glazunov et al., 2012). However, it is in general not fully possible to know exactly what channel model is the typical or the most representative one. On the other hand, it is often useful to look at phenomena in the limiting cases to model and understand certain phenomena, for example, by looking into the static or the high frequency limits.

In wireless communications, the Rich Isotropic MultiPath (RIMP) propagation channel and the Line-of-Sight (LOS) propagation channel represent two limiting propagation environments in terms of the spatial distribution of the angle-of-arrival (AoA) or angle-of-departure (AoD). As argued in Björnson et al. (2016) and Ngo et al. (2014), both channels are favorable for the operation of Massive MIMO. Therefore, it is reasonable to expect that real propagation environments, which are likely to be in-between these extremes, would also be favorable. This has support from experimentally observed FP characteristics of Massive MIMO channels in real life (Gao et al., 2015).

This fact has a very profound implication; that is, both the RIMP and the LOS environments may suffice to characterize the Over-The-Air (OTA) performance of wireless devices as suggested in Kildal (2013). The following *real-life hypothesis* for OTA device characterization has been formulated as follows: *if a wireless device is proven to work well in RIMP and Random-LOS, it will work well in all real-life environments*

(Kildal & Carlsson, 2013). It is worthwhile to note that the Random-LOS propagation environment is a generalization of the LOS environment concept, where the randomness is a result of the unpredictable positions and orientations of antennas of the mobile stations (Glazunov & Lehne, 2018; Lehne et al., 2015), the deployment position of a RBS, or both. In Random-LOS, both the AoA and the polarization of the LOS wave (i.e., the only wave present) are considered to be random variables (Razavi et al., 2016).

The RIMP and the Random-LOS environments are especially relevant to the OTA characterization of Massive MIMO RBS in 5G wireless systems. 5G massive array antennas will, in practice, be only possible to measure in OTA setups due to the large number of ports. Moreover, as we go higher in frequency, for example, for systems operating at mm-wave frequencies, there will be most likely no access to measurement ports at all.

Here we therefore present an investigation of the impact of scattering on the signal fading statistics as a function of frequency from 500 MHz to 100 GHz. We neglect the water vapor and oxygen absorption effects as well as the propagation mechanisms leading to large-scale signal fading fluctuations. We assume that these will occur on top of the presented scattering model. We develop a model for signal fluctuations due to scattering, that is, short-term fading, as a function of frequency under various simplifying assumptions. The main idea is to be able to provide an analytical model able to capture both the antenna characteristics as well as the impact of scatterers on the short-term signal fluctuations. The model offers to investigate the impact of the size of the scattering environment, the scatterer density, the number of scatterers, and the scatterer type (through the average scattering cross section), on the signal fading (i.e., signal variability), for example, as a function of frequency. The model is general in the sense that it is not derived for specific type of scatterers; however, clearly some specific assumptions have been made to allow for analytical tractability. For illustrative purposes we further specialize the scatterers to be emulated by resonant dipoles. The obtained analytical model is then compared to numerical computations performed with functions inherited from the CAESAR code (Maaskant, 2010). Under the specific assumptions used in the example, it is shown that as we go higher in frequency, the power in the LOS component gradually increases as compared to the power of the scattering contribution. This phenomenon has recently been observed in measurements as well (Haneda et al., 2017). Hence, under certain conditions and for a fixed number of thin wire scatterers, the scattering environment behaves like the RIMP channel at lower frequencies, while at higher frequencies it becomes more like the (Random-)LOS channel. However, given the complexity of the problem at hand further investigations need to be performed that also cover a different frequency dependence behavior. However, to the best knowledge of the authors no such scatterer model exists yet, but it can therefore be a part of future investigations.

The paper is organized as follows. In section 2 the signal fading model and Rician K -factor are defined. Then, the scattering model and all assumptions for this model are presented in section 3. The detailed derivation of K -factor as a function of the average scattering cross section of scatterers is provided in section 4. The results from the analytical K -factor computations and a MoM numerical simulations for different cases are compared in section 5, with discussions and analysis on the results. Finally, the paper is concluded in section 6.

2. Signal Fading Model

To study the scattering environment, let us assume a transmitter and a receiver antenna in the presence of scatterers as illustrated in Figure 1. In order to model the single-port receive signal we introduce the complex random variable

$$v = \frac{V_{oc}}{2\sqrt{2R_{ar}}}, \quad (1)$$

where V_{oc} is the *total* open-circuit voltage induced at the receive antenna ports and R_{ar} is the real part of the receive antenna input impedance. The received power as a function of the open-circuit voltage for the conjugate-matched load condition is

$$P_{ar} = |v|^2 = \frac{|V_{oc}|^2}{8R_{ar}}. \quad (2)$$

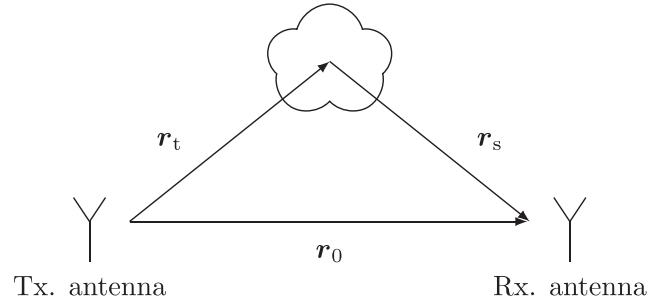


Figure 1. Transmitter and receiver antennas in the scattering environment.

Scattering describes three main physical propagation mechanisms, that is, reflection, refraction, and diffraction, and can be specular or diffuse. Especially, a dominating propagation mechanism in wireless multipath channels is diffuse scattering (Glazunov et al., 2012). Objects (scatterers) surrounding the mobile antenna are assumed to contribute the most to the fast fading (short-term) fluctuations of the received signal (Jakes, 1974). Hence, we seek to estimate the impact of the scattering on the fast fading process as a function of frequency. It is important to note that diffuse scattering mechanism is not explicitly modelled in this paper, but its effect is characterized through the average scattering cross section of the scatterers.

The Rician probability distribution function (pdf) has gained widespread acceptance as a model of the continuous wave signal fluctuations caused by multipath propagation. A measure of the severity of fluctuations is then given by the Rician K -factor defined as

$$K = \frac{P_{\text{LOS}}}{P_{\text{RIMP}}} = \frac{|\langle v \rangle|^2}{\langle |v|^2 \rangle - |\langle v \rangle|^2}, \quad (3)$$

where P_{LOS} and P_{RIMP} are the powers of the LOS and the RIMP components, respectively, and $\langle v \rangle$ denotes the ensemble average of complex-valued random variable v .

The second parameter that defines the Rician pdf is the total received power

$$P_r = P_{\text{LOS}} + P_{\text{RIMP}} = \langle |v|^2 \rangle. \quad (4)$$

The Rician distribution of the envelope of the complex signal amplitude received by the antenna $|v|$ is given by (Jakes, 1974),

$$f_{|v|}(|v|) = \frac{2(1+K)|v|}{P_r} \exp\left(-K - \frac{(K+1)|v|^2}{P_r}\right) \times I_0\left(2\sqrt{\frac{K(1+K)}{P_r}}|v|\right), \quad (5)$$

where I_0 is the modified Bessel function of the first kind and zeroth order.

The physical interpretation of (3) is that the receive signal fading, or severity of fluctuations, is a function of the proportion between the power of the deterministic component of the received signal, that is, given by the numerator and the power in the stochastic component, that is, given by the denominator. The former can be interpreted as the LOS field component while the latter can be interpreted as the RIMP component. Two limiting cases immediately arise, that is, $K \rightarrow 0$ and $K \rightarrow \infty$ denoting the RIMP and the LOS channels, respectively. Thus, intermediate values of K will describe Rician propagation channels in between the RIMP and the LOS channels. It is worthwhile to note that in practice, the deterministic component can be just a strong reflected or diffracted wave, while the stochastic component not necessarily arises from an isotropic wave field distribution. For the sake of simplicity we will not consider this general case. Instead, we will look into the situation when there is a LOS field component in addition to a RIMP field component.

3. Scattering Model and General Assumptions

In wireless communication channels, as well as in microwave sensing or radar applications (Shi et al., 2017), there is usually more than one single scatterer interacting with the receive and transmit antennas. Many

scatterers have to be considered in order to completely define the propagation channel. However, in practice, full knowledge about the exact physical properties and positions of the scatterers is not available. Here, we are mainly concerned with the statistical modeling of the channel, an approach that has gained widespread use in wireless communication (Molisch, 2012) and remote sensing applications (Tsang et al., 2004). For this reason, the antennas and scatterers are assumed to be in the far-field region of each other, and single scattering is assumed.

To fully and exactly evaluate the scattering contribution to the total received signal is a too complex task to accomplish even under the assumptions already stated above. We need therefore to introduce further assumptions. The total open-circuit voltage entering (1) is a random variable due to the random nature of the scattered field component as shown further below. The randomness arises from the random positions of the scatterers relative to each other and the antennas. In turn, this results in the polarization of the scattered waves behaving like a random process too. Also the phase difference can be considered random due to different path lengths traveled by the scattered waves.

In a real scattering environment, the different scattering objects (scatterers) will appear to have different sizes depending on the frequency. For example, it is expected that small scatterers can become more directive reflectors at high frequencies, and the dense multipath component can decrease with frequency. Also the electrical distance between scatterers will increase with frequency. Moreover, different parts of a larger scatterer may be modeled by a set of smaller scatterers with no electrical coupling to each other under the approximations assumed herein. Small half-wavelength dipole antennas have been used to model the electromagnetic scattering in wireless channels in Bialkowski et al. (2006). Herein, we adopt a similar approach. Before we proceed further, let us summarize our simplifying modeling assumptions:

- (I) We consider a narrowband continuous wave signal.
- (II) Antennas and scatterers are in the far-field of each other, where the far-field reference distance is given by R_{FF} computed according to the criterion given in Kim et al. (2013).
- (III) For the sake of simplicity, we assume that the scatterers are uniformly distributed within a spherical scattering volume. The probability distribution of a scatterer being located ρ from the center of a sphere of radius R_s or at the angle θ is given by

$$p(\rho) = \frac{3\rho^2}{R_s^3}, \quad (6a)$$

$$p(\theta) = \frac{\sin \theta}{2}, \quad (6b)$$

respectively, where the radius R_s delimits the volume containing the scatterers. Furthermore, the receiver antenna is located at the center of the volume.

- (IV) We assume that the transmit antenna is far away from the scattering volume, while the receive antenna is within the scattering volume at $\rho = 0$. The communication scenario assumes a local cloud of scatterers surrounding the mobile user, which is distant to the base station antenna and therefore illuminated uniformly by a plane wave.
- (V) Only single scattering is considered in our analytical model. However, in the later MoM simulations multiple scattering is included.
- (VI) The scattering contribution of the scatterers is determined by their spatially averaged scattering cross section.
- (VII) The randomness in the positions of scatterers is assumed to originate from an ensemble of states originating from a random process.

It is worth pointing out that because our assumed channel model is simple in nature it can only predict dominant effects and thus general qualitative trends, such as the indication that the Rician K -factor increases with frequency, which is a phenomenon that has recently been observed in measurements as well (Haneda et al., 2017). However, to predict more quantitatively what happens in other communication scenarios as well as in more specific environments, we refer, for example, to previous studies (Ghoraishi et al., 2006; Riaz et al., 2015; Samimi & Rappaport, 2016).

4. Computation of K -Factor and P_r

Consider the following scattering problem where the field radiated by a transmit antenna is scattered by a single linear scatterer. We are then interested in computing the total field propagating towards the receive

antenna. The geometry of the problem is illustrated in Figure 1. The field radiated by the transmit antenna $\mathbf{E}_d(\mathbf{r}_t)$ is defined in the far-field region by the far-field function $\mathbf{G}_t(\hat{\mathbf{r}}_t)$ radiated in direction $\hat{\mathbf{r}}_t = \mathbf{r}_t/r_t$ as

$$\mathbf{E}_d(\mathbf{r}_t) = \mathbf{G}_t(\hat{\mathbf{r}}_t) \frac{e^{-jk r_t}}{r_t} + \mathcal{O}(r_t^{-2}) \text{ as } r_t \rightarrow \infty, \quad (7)$$

where $\mathcal{O}(x^n)$ stands for “order of” asymptotic. This is the field impinging on the scatterer.

Similarly, in the far-field region, the scattered electric field \mathbf{E}_s is fully described by the far-field function \mathbf{G}_s scattered in direction $\hat{\mathbf{r}}_s = \mathbf{r}_s/r_s$ as

$$\mathbf{E}_s(\mathbf{r}_s) = \mathbf{G}_s(\hat{\mathbf{r}}_s) \frac{e^{-jk r_s}}{r_s} + \mathcal{O}(r_s^{-2}) \text{ as } r_s \rightarrow \infty, \quad (8)$$

where \mathbf{G}_s can be expressed in terms of the scattering matrix $S(\hat{\mathbf{r}}_s, \hat{\mathbf{r}}_t)$ (Van Bladel, 2007)

$$\mathbf{G}_s(\hat{\mathbf{r}}_s) = S(\hat{\mathbf{r}}_s, \hat{\mathbf{r}}_t) \cdot \mathbf{E}_d(\mathbf{r}_t), \quad (9)$$

where we have assumed that the amplitude of the plane wave incident at the scatterer from direction $\hat{\mathbf{r}}_t$ is given by $\mathbf{E}_d(\mathbf{r}_t)$. Hence, from (7)–(9), the scattered field can be expressed as

$$\mathbf{E}_s(\mathbf{r}_s) = S(\hat{\mathbf{r}}_s, \hat{\mathbf{r}}_t) \cdot \mathbf{G}_t(\hat{\mathbf{r}}_t) \frac{e^{-jk(r_s+r_t)}}{r_s r_t} \text{ as } r_s, r_t \rightarrow \infty. \quad (10)$$

The total field impinging on the receive antenna will then be the sum of the scattered field (10) and the field radiated by the antenna (7) in the direction of vector \mathbf{r}_o

$$\mathbf{E}_{\text{tot}} = \mathbf{E}_d(\mathbf{r}_o) + \mathbf{E}_s(\mathbf{r}_s). \quad (11)$$

The open-circuit voltage induced at the receive antenna ports by an impinging wave is given by (Kildal, 2015)

$$V_{\text{oc}}^{\text{tot}} = \frac{2\lambda}{j\eta l} \mathbf{G}_r \cdot \mathbf{E}_{\text{tot}}, \quad (12)$$

where \mathbf{G}_r is the far-field function of the receive antenna in the direction $\hat{\mathbf{r}}$ for excitation current I and \mathbf{E}_{tot} the amplitude of the incident plane wave field measured at the phase center of the receive antenna that we choose to be the origin of the coordinate system associated with that antenna.

From (11) and (12) we see that the total open-circuit voltage can be expressed as the sum of two terms

$$V_{\text{oc}}^{\text{tot}} = V_{\text{oc}}^{\text{d}} + V_{\text{oc}}^{\text{s}}, \quad (13)$$

where both terms are obtained from the corresponding terms in (11), that is, induced by the direct field and the scattered field, respectively.

We consider next the situation when many scatterers are present between the transmit and the receive antennas. The scatterers and the antennas have associated with them local coordinate systems, while their relative positions are defined relative to a common coordinate system. Single scattering (no coupling between the scatterers) is assumed, unlike in the later MoM simulations. Enforcing the above made assumptions gives after some algebraic manipulations the following expression for the open-circuit voltage induced by N_s scatterers:

$$V_{\text{oc}}^{\text{s}} = \frac{2\lambda}{j\eta l} \sum_{n=1}^{N_s} \mathbf{G}_r(\hat{\mathbf{r}}_{rn}) \cdot S_n(-\hat{\mathbf{r}}_{rn}, \hat{\mathbf{r}}_{tn}) \cdot \mathbf{G}_t(\hat{\mathbf{r}}_{tn}) \frac{e^{-jk(r_{rn}+r_{tn})}}{r_{rn} r_{tn}}, \quad (14)$$

where we use the radius-vector notation introduced in Figure 1. We have also introduced the subindex n in the scattering matrix to indicate that scatterers are in general different. The open-circuit voltage for the direct wave is given by

$$V_{\text{oc}}^{\text{d}} = \frac{2\lambda}{j\eta l} \mathbf{G}_r(-\hat{\mathbf{r}}_o) \cdot \mathbf{G}_t(\hat{\mathbf{r}}_o) \frac{e^{-jk r_o}}{r_o}. \quad (15)$$

Under the assumptions stated above, (13)–(15) provide a rather general description of the signal scattering model satisfying the above-stated assumptions.

In order to evaluate (3), we need to evaluate $\langle V_{oc}^{tot} \rangle$ and $\langle |V_{oc}^{tot}|^2 \rangle$ first. As can be seen from (14), $\langle V_{oc}^{tot} \rangle = \langle V_{oc}^s \rangle + V_{oc}^d$. Hence, we need to find

$$\langle V_{oc}^s \rangle = \sum_{n=1}^{N_s} \left\langle \frac{2\lambda}{j\eta I} \mathbf{G}_r \cdot \mathbf{S}_n \cdot \mathbf{G}_t \right\rangle \left\langle \frac{e^{-jk(r_{rn}+r_{tn})}}{r_{rn}r_{tn}} \right\rangle, \quad (16)$$

where we have omitted the arguments of some functions for the sake of simplicity. Observe that the ensemble averaging has been factored into two terms: (i) a term that comprises the scattering matrix, which describes randomness of the scattered field polarization and AoA at the location of the receiver antenna, and (ii) a term comprising the random positions of the scatterers. Both are independent random processes. We immediately see that

$$\langle V_{oc}^s \rangle = 0, \quad (17)$$

since both ensemble averages are zero as shown in Appendix A. Hence, we obtain that

$$\langle V_{oc}^{tot} \rangle = V_{oc}^d. \quad (18)$$

Then from (2), (15), and the Friis equation (Kildal, 2015) we arrive at

$$P_{LOS} = \frac{|V_{oc}^{tot}|^2}{8R_{ar}} = \frac{|V_{oc}^d|^2}{8R_{ar}} = \left(\frac{\lambda}{4\pi r_o} \right)^2 G_{or} G_{ot} P_t, \quad (19)$$

where G_{or} and G_{ot} are the gains of the receive and transmit antennas in the LOS direction and P_t is the transmit power.

We see from (13) and (17) that

$$\langle |V_{oc}^{tot}|^2 \rangle = \langle |V_{oc}^s|^2 \rangle + |V_{oc}^d|^2. \quad (20)$$

Hence, we need to find

$$\begin{aligned} \langle |V_{oc}^s|^2 \rangle &= \sum_{n=1}^{N_s} \sum_{n'=1}^{N_s} \left\langle \left(\frac{2\lambda}{\eta I} \right)^2 (\mathbf{G}_r \cdot \mathbf{S}_n \cdot \mathbf{G}_t) (\mathbf{G}_r \cdot \mathbf{S}_{n'} \cdot \mathbf{G}_t)^* \right\rangle \times \\ &\quad \left\langle \frac{e^{-jk(r_{rn}+r_{tn}-r_{rn'}-r_{tn'})}}{r_{rn}r_{tn}r_{rn'}r_{tn'}} \right\rangle, \end{aligned} \quad (21)$$

After taking into account the random position of scatterers and the antenna parameters conventions and definitions in Kildal (2015) we show in Appendix B that

$$P_{RIMP} = \frac{\langle |V_{oc}^s|^2 \rangle}{8R_{ar}} = \frac{3N_s}{4\pi R_s^2} \left(\frac{\lambda}{4\pi r_o} \right)^2 e_r G_{ot} \langle \sigma_s \rangle P_t, \quad (22)$$

where e_r is the radiation efficiency of the receive antenna; all the other variables have been defined above.

Combining (19) and (22) into (3) we obtain an estimate of the frequency dependence of the K -factor as function of frequency

$$K(f) = \frac{8\pi D_{or} R_s^2}{3N_s \langle \sigma_s \rangle}, \quad (23)$$

where we have used the relationship between antenna gain and directivity $G_{or} = e_r D_{or}$. Under the above assumptions, the frequency dependence of the K -factor is completely determined by the directivity of the receiver antenna and the type of scatterer used in the model, that is, the corresponding $\langle \sigma_s \rangle$. Expression (23) describes the dependence of the K -factor on the radius of the scattering volume R_s for constant N_s . Clearly, in this case the scatterers will be further away from the receiving antenna if R_s increases. This leads to a weaker contribution to the total scattered field power and therefore a predominance of the LOS component over the RIMP component, that is, a larger K -factor.

Let us now keep the scatterer density $\rho_s = N_s/V_s$ constant, where $V_s = 4\pi R_s^3/3$. Then, the K -factor can be written as

$$K(f) = \frac{2D_{\text{or}}}{\rho_s R_s \langle \sigma_s \rangle}. \quad (24)$$

In this case, the trend is the opposite. Indeed, keeping the density constant, a larger radius of the scattering volume will result in a smaller K -factor due to the larger contribution of the RIMP component to the total received power as compared to the LOS component.

Results (23) and (24) are both obtained under the assumption that all scatterers and the antennas are in the far-field of each other. Now, for a fixed R_s there will be a maximum number of scatterers N_s that can be “packed” into this volume. To obtain this estimate we use the far-field distance R_{FF} to model the diameter of an imaginary sphere surrounding the scatterer. Hence, we need to estimate the number of spheres with volume $V_{\text{FF}} = \pi R_{\text{FF}}^3/6$ that can be packed into the volume containing the scatterers $V_s = 4\pi R_s^3/3$. This number is given by

$$N_s = \frac{\eta_{\text{pack}} V_s}{V_{\text{FF}}} = 8\eta_{\text{pack}} \left(\frac{R_s}{R_{\text{FF}}} \right)^3, \quad (25)$$

where $\eta_{\text{pack}} \approx 0.64$ is the packing density of random close packing of spheres (Jaeger & Nagel, 1992). The corresponding scatterer density becomes

$$\rho_s = \frac{N_s}{V_s} = \frac{6\eta_{\text{pack}}}{\pi R_{\text{FF}}^3}. \quad (26)$$

Thus, (23) and (24) both reduce to

$$K(f) = \frac{\pi D_{\text{or}} R_{\text{FF}}^3}{3\eta_{\text{pack}} R_s \langle \sigma_s \rangle}, \quad (27)$$

which provides a lower bound on the K -factor in the scattering propagation environment described above. It is worthwhile to note that the far-field distance R_{FF} also depends on the frequency (Kim et al., 2013)

$$R_{\text{FF}} = \frac{4\lambda G_o}{\pi^2} \sqrt{\frac{\alpha_E}{1 - \gamma_A}}, \quad (28)$$

where λ is the wavelength, G_o is the antenna gain, $\alpha_E = 0.06$ is a fitting coefficient that is the same for all antennas, and γ_A is the antenna gain reduction factor defined by the user. The starting point of the corresponding far-field region for a required error magnitude of the antenna gain is defined by $1 - \gamma_A$.

It must be noted that the above results are rather general with respect to the choice of scatterers (still satisfying the above assumptions). Hence, depending on the frequency dependence of both scatterers and the antenna used, a different behavior of the K -factor can be obtained. Even if closed-form expressions are given, no closed-form expressions of directivity are known for all antennas nor the spatially averaged scattering cross sections for all scatterers are known. These can be obtained either experimentally or numerically following the needs of the user of the model and hence the semi-analytical description of the presented model.

5. Results

5.1. Specific Assumptions

For the results in this section, we specialize our scatterers to identical dipoles. The scatterers are assumed to be identical vertically polarized resonant dipoles. The spatially averaged scattering cross section of dipoles is given as (Peebles, 1984)

$$\frac{\langle \sigma_{\text{dip}} \rangle}{\lambda^2} = \frac{1.178 \frac{L}{\lambda} + 0.179 \ln(22.368 \frac{L}{\lambda}) - 0.131}{\ln^2(22.368 \frac{L}{\lambda})}, \quad (29)$$

Table 1
Spatially Averaged Scattering Cross-Section of Dipole of Length L

L/λ	0.5	1.5	2.5	3.5	4.5
$\langle \sigma_{\text{dip}}/\lambda^2 \rangle$	0.1527	0.1835	0.2183	0.2510	0.2819

where $L = n\lambda/2$, $n = \{1, 2, \dots\}$, and λ is the free-space wavelength. Values of the averaged cross section for different lengths of dipole that are used in the results in this section are summarized in Table 1.

Assuming $R_s = 15$ m, the lower bound of the K -factor according to (27) is plotted in Figure 2 versus frequency, for different electrical lengths of the scatterers. It can be observed that with the increase in frequency, a larger number of scatterers can fit in the volume (according to 28) which results in the increase of the scattered power and the decrease of the K -factor. On the other hand, the larger electrical size of the scatterers leads to increased K -factor, since it means that a smaller number of scatterers can fit in the volume. However, if the number of scatterers is kept constant, the K -factor will increase with frequency. This is shown in Figure 2 with the dash-dotted curves, where the spacing between the scatterers is chosen according to the R_{FF} value at the lowest frequency, that is, 500 MHz. Note that in this case N_s is dependent on the electrical size of the scatterers. We can also assume a case where a fixed N_s is chosen for all values of the electrical length. This case is shown in Figure 2 with the solid lines for $N_s = 1,000$. Unlike the previous cases, as expected, we observe in this case that larger electrical size will lead to lower K -factor.

5.2. Comparison With Numerical MOM-Based Simulations

We have used MoM in order to numerically simulate the model. Effects of multiple scattering and mutual coupling between the scatterers are included in the full-wave simulations. The scatterers are modeled as half-wave PEC strips of $\lambda/100$ width, which are uniformly distributed in a cubic volume with side length of 30 m. Assuming the transmitter antenna is located far from the scatterers and the receiver antenna, it is modeled as a plane wave impinging on the volume. Furthermore, in order to remove the effect of the receiver antenna's radiation pattern, it is assumed to be an ideal omnidirectional vertically polarized antenna. This implies that in the simulations, the vertical component of the field is studied, and in the model we have $D_{\text{or}} = 1$. Finally, in order to reduce the computation time, Characteristic Basis Functions Method (CBFM) is employed for the resonant scatterers (Maaskant, 2010). The position of the scatterers are randomized 20 times. With each set of positions, the fields are calculated at $11 \times 11 \times 11 = 1,331$ points in the center of the scattering environment. The average of all these values is then used in the plots.

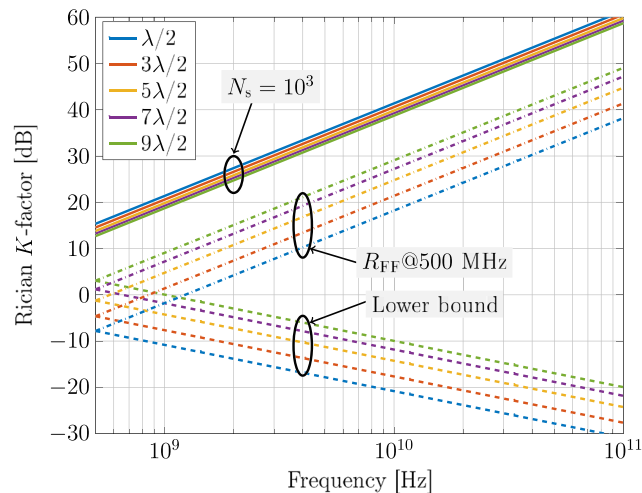


Figure 2. The Rician K -factor versus frequency for different electrical lengths of the scatterers in a volume with $R_s = 15$ m. Three different scenarios: (1) the lower bound, where the scattering volume is filled with largest possible number of scatterers where all of them are in the far-field region of each other; (2) the spacing between the scatterers is chosen based on the far-field distance (R_{FF}) at the lowest frequency; and (3) a fixed number of scatterers randomly distributed in the scattering environment, regardless of the electrical size.

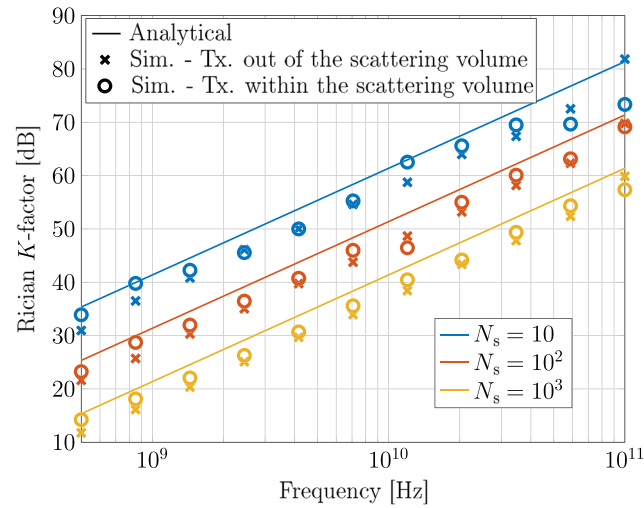


Figure 3. Comparison of analytical and simulated K -factor versus frequency, for different numbers of identical vertical resonant scatterers. Simulated K -factor for the case of transmitter antenna located in the scattering volume is plotted with dashed line.

Figure 3 shows the analytical and simulated K -factor for cases of 10, 100, and 1,000 scatterers in the frequency range from 500 MHz up to 100 GHz. It is observed that the simulations and analytical formulas follow the same trend. However, the K -factor in the analytical model is slightly larger than the simulation results. This can be explained by the fact that the analytical model assumes only single scattering, whereas the effect of multiple scattering is included in the simulation results. It is worthwhile to note that an improvement of the presented model can result from modelling the coupling between scatterers. However, that is more complex problem that is outside the scope of the presented work. Another source of error can be the fact that the density of the scatterers is lower in the cubic volume than the spherical one. We observe that for a fixed number of scatterers, the K -factor increases with frequency, meaning that the LOS component becomes more dominant at the higher frequencies for this specific scenario.

So far, we have made the assumption that the transmitter antenna is further away from the scattering volume. However, we can also assume it to be located in the scattering volume among the scatterers. We simulate the transmitter as a half-wave dipole located at $R_t = R_s/2 = 7.5$ m. The other details of the simulation are kept as before. The simulated K -factor for this scenario is also plotted in Figure 3. We observe that while the K -factor has slightly increased, the trend of its frequency dependence does not change. Table 2 summarizes the root-mean-square deviation of the K -factor values in dB, between the analytical model and the two cases in MoM simulations.

In addition to the case of half-wave PEC scatterers, we have considered two other cases in the MoM simulations for the sake of comparison. In one case, scatterers are loaded with a matched load in order to absorb part of the radiated field from the transmitter antenna and to reduce the scattered power. In the second case, a number of $2\lambda \times 2\lambda$ PEC plates are also distributed among the half-wave dipoles, in order to increase the scattered power. In this case, the number of PEC plates is 1, 5, and 20 in the cases where N_s is 10, 100, and 1,000, respectively. Sixty-three characteristic basis functions are used for each plate. The K -factor is plotted versus frequency for these three cases in Figure 4. As expected, we observe in this figure that for the same N_s , terminating the dipole in matched load will lead to higher K -factor, while the presence of the PEC plates

Table 2
Root-Mean-Square Deviation of the K -Factor in dB, for the Analytical Model Compared to MoM Results

N	10	100	1,000
Tx. out of the scattering volume	3.8	4.0	4.0
Tx. within the scattering volume	3.9	3.1	2.8

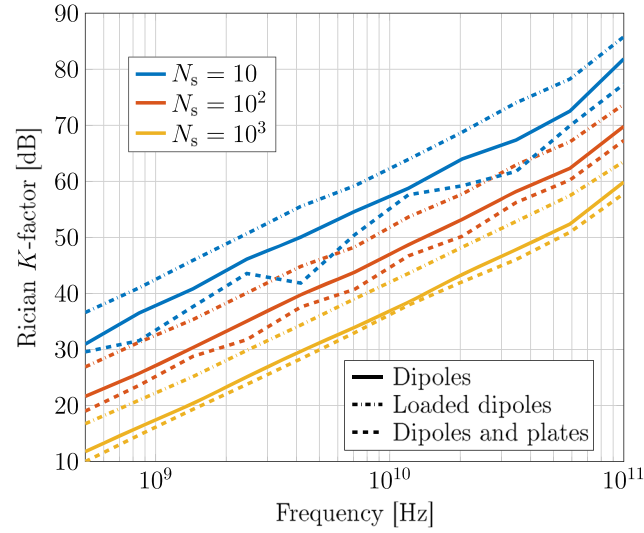


Figure 4. The simulated Rician K -factor in the presence of PEC plate scatterers and match-loaded half-wave dipoles.

leads to decreased K -factor. However, we observe that the general trend of the K -factor versus frequency is the same for all cases.

6. Conclusions

A semi-analytical model is introduced to investigate the frequency dependence of Rician K -factor in generic random scattering environments. The K -factor is derived analytically as a function of the average scattering cross section of the scatterers. The formulas are verified against full-wave MoM simulations which shows a good agreement between the two. The main contributing factors to the K -factor are shown to be the density of the scatterers ρ_s , the radius of the scattering environment R_s , the average bistatic cross section of the scatterers $\langle \sigma_s \rangle$, and the directivity of the receiving antenna D_{or} . Of these, $\langle \sigma_s \rangle$ and D_{or} are frequency dependent and contribute to the frequency dependence of the K -factor. In the simulations two scenarios are investigated with the transmitter antenna both within the scattering volume and out of it. It is observed that for thin wire scatterers and planar scatterers, the K -factor increases quadratically with the frequency. Although we have used resonant dipoles in the model, the formulas have the flexibility to accommodate other types of scatterers as long as the average cross section is known from either numerical computations or measurements.

As a final remark we may say that the model presented here needs further study to take into account other specific propagation scenarios of great relevance known as obstructed line-of-sight and the more general ones described as non-line-of-sight scenarios. Specific applications such as vehicle-to-vehicle or Massive MIMO systems need to be studied too. Also various aspects of the computational efficiency of models need to be addressed in future work.

Appendix A: Support to the Derivation of the LOS Contribution

Although the scatterers are assumed to have same orientation, and due to their random positions, the polarization vector $\hat{\mathbf{p}}_s$ of the scattered field impinging on the receive antenna will be randomly mismatched to its polarization vector $\hat{\mathbf{p}}_r$, where $\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s$ is the mismatch angle. We have

$$\begin{aligned} \left\langle \frac{2\lambda}{j\eta l} \mathbf{G}_r \cdot \mathbf{S}_n \cdot \mathbf{G}_t \right\rangle &= \left\langle \frac{2\lambda}{j\eta l} |\mathbf{G}_r| |\mathbf{S}_n \cdot \mathbf{G}_t| \cos(\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s) \right\rangle \\ &= \left\langle \frac{2\lambda}{j\eta l} |\mathbf{G}_r| |\mathbf{S}_n \cdot \mathbf{G}_t| \right\rangle \langle \cos(\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s) \rangle \\ &= 0, \end{aligned} \quad (\text{A1})$$

since $\langle \cos(\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s) \rangle = 0$ for $\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s$ uniformly distributed between 0 and 2π .

In order to show that the second ensemble average is also zero we now make further assumptions that simplify our computations

$$r_{tn} \approx r_o, \quad (\text{A2a})$$

$$r_{tn} = \rho_n, \quad (\text{A2b})$$

where (A2a) states that the transmit antenna is at a much larger distance from both the receive antenna and the scatterer as compared to the radius R_s that delimits the volume containing the scatterers. (A2b) is just a substitution of variables. Hence, we can now write

$$\left\langle \frac{e^{-jk(r_{tn}+r_{tn})}}{r_{tn}r_{tn}} \right\rangle \approx \frac{1}{r_o} \left\langle \frac{e^{-jk r_{tn}} e^{-jk \rho_n}}{\rho_n} \right\rangle. \quad (\text{A3})$$

Without losing generality, we assume the local coordinate system on the receiver antenna is chosen such that the transmitter antenna is located at $\theta = 0$ and the n th scatterer is located at θ_n . Then, (A3) is approximated as

$$\begin{aligned} \frac{1}{r_o} \left\langle \frac{e^{-jk r_{tn}} e^{-jk \rho_n}}{\rho_n} \right\rangle &\approx \frac{1}{r_o} \left\langle \frac{e^{-jk(r_o - \rho_n \cos \theta_n)} e^{-jk \rho_n}}{\rho_n} \right\rangle \\ &= \frac{e^{-jk(r_o)}}{r_o} \left\langle \frac{e^{-jk \rho_n(1 - \cos \theta_n)}}{\rho_n} \right\rangle, \end{aligned} \quad (\text{A4})$$

where, using (6b), it can be shown after straightforward algebraic manipulations that

$$\begin{aligned} \left\langle \frac{e^{-jk \rho_n(1 - \cos \theta_n)}}{\rho_n} \right\rangle &= \int_{\rho=0}^{R_s} \int_{\theta=0}^{\pi} \frac{e^{-jk \rho(1 - \cos \theta)}}{\rho} \frac{3\rho^2 \sin \theta}{R_s^3} d\theta d\rho \\ &= 0 + \mathcal{O}(R_s^{-2}) \text{ as } R_s \rightarrow \infty. \end{aligned} \quad (\text{A5})$$

In practice, it suffices that $R_s \gg \frac{\lambda}{2\pi}$.

Appendix B: Support to the Derivation of the RIMP Contribution

Let us first recall some antenna parameters following the definitions in Kildal (2015). The directivity of an antenna is defined as

$$D_o(\hat{\mathbf{r}}) = \frac{4\pi |\mathbf{G}(\hat{\mathbf{r}})|^2}{2\eta P_{\text{rad}}}, \quad (\text{B1})$$

where $\mathbf{G}(\hat{\mathbf{r}})$ is the far-field function satisfying the normalization integral

$$\oint D_o(\hat{\mathbf{r}}) d\Omega = \oint \frac{4\pi |\mathbf{G}(\hat{\mathbf{r}})|^2}{2\eta P_{\text{rad}}} d\Omega = 4\pi. \quad (\text{B2})$$

The total radiated power is

$$P_{\text{rad}} = e_{\text{rad}} P_t, \quad (\text{B3})$$

where e_{rad} is the radiation efficiency of the antenna and P_t is the input power to the antenna, which, in turn, is related to the current at the antenna input port $|I|$ (in 12) as

$$P_t = \frac{1}{2} R_{\text{ar}} |I|^2. \quad (\text{B4})$$

The antenna gain is given by

$$G_o = e_{\text{rad}} D_o. \quad (\text{B5})$$

Following the assumption that the polarization of the scattered field at the position of the receiver antenna is random, we write the ensemble average of $|V_{oc}^s|^2$ as

$$\begin{aligned} \langle |V_{oc}^s|^2 \rangle &= \sum_{n=1}^{N_s} \sum_{n'=1}^{N_s} \left\langle \left(\frac{2\lambda}{\eta|I|} \right)^2 (\mathbf{G}_r \cdot \mathbf{S}_n \cdot \mathbf{G}_t) (\mathbf{G}_r \cdot \mathbf{S}_{n'} \cdot \mathbf{G}_t)^* \right\rangle \\ &\quad \times \left\langle \frac{e^{-jk(r_{rn}+r_{tn}-r_{rn'}-r_{tn'})}}{r_{rn}r_{tn}r_{rn'}r_{tn'}} \right\rangle \\ &= \sum_{n=1}^{N_s} \left\langle \left(\frac{2\lambda}{r_o\eta|I|} \right)^2 |\mathbf{G}_r \cdot \mathbf{S}_n \cdot \mathbf{G}_t|^2 \right\rangle \left\langle \frac{1}{\rho_n^2} \right\rangle, \end{aligned} \quad (B6)$$

where we have used the results in Appendix A; that is, for $n \neq n'$ the ensemble averages are null. All the terms in (B6) are identical since the scatterers are identical.

Let us denote the first ensemble average in (B6) by X , then

$$\begin{aligned} X &= \left\langle \left(\frac{2\lambda}{r_o\eta|I|} \right)^2 |\mathbf{G}_r \cdot \mathbf{S}_n \cdot \mathbf{G}_t|^2 \right\rangle \\ &= \left\langle \left(\frac{2\lambda}{r_o\eta|I|} \right)^2 |\mathbf{G}_r|^2 |\mathbf{S}_n \cdot \mathbf{G}_t|^2 \cos^2(\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s) \right\rangle \\ &= \left\langle \left(\frac{2\lambda}{r_o\eta|I|} \right)^2 |\mathbf{G}_r|^2 \right\rangle \langle |\mathbf{S}_n \cdot \mathbf{G}_t|^2 \rangle \langle \cos^2(\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s) \rangle, \end{aligned} \quad (B7)$$

where the factorization of the ensemble average has been performed by grouping terms that are statistically independent.

The bistatic scattering cross section is defined as

$$\sigma(-\hat{\mathbf{r}}_{tn}, \hat{\mathbf{r}}_{tn}) = 4\pi \frac{|\mathbf{S}_n(-\hat{\mathbf{r}}_{tn}, \hat{\mathbf{r}}_{tn}) \cdot \mathbf{G}_t|^2}{|\mathbf{G}_t|^2}. \quad (B8)$$

Then, inserting (B8) into (B7) gives

$$X = \left\langle \left(\frac{2\lambda}{r_o\eta|I|} \right)^2 |\mathbf{G}_r|^2 \right\rangle \frac{\langle \sigma \rangle}{4\pi} \langle |\mathbf{G}_t|^2 \rangle \langle \cos^2(\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s) \rangle. \quad (B9)$$

We now compute the ensemble average terms in (B7). Since we assume that $\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s$ is uniformly distributed between 0 and 2π , then

$$\langle \cos^2(\angle \hat{\mathbf{p}}_r \hat{\mathbf{p}}_s) \rangle = \frac{1}{2}. \quad (B10)$$

Given assumption (A2a), we use (B1), (B3), and (B5) to arrive at

$$\langle |\mathbf{G}_t|^2 \rangle \approx |\mathbf{G}_t|^2 = \frac{2\eta G_{ot} P_t}{4\pi}. \quad (B11)$$

Combining (B2)–(B4) into the first ensemble average in (B9) we get

$$\left\langle \left(\frac{2\lambda}{r_o\eta|I|} \right)^2 |\mathbf{G}_r|^2 \right\rangle = \left\langle \left(\frac{2\lambda}{r_o\eta} \right)^2 \frac{e_{rad} R_{ar} |\mathbf{G}_r|^2}{2P_{rad}} \right\rangle, \quad (B12a)$$

$$= \frac{8R_{ar} e_{rad}}{2\eta} \left(\frac{\lambda}{r_o} \right)^2 \left\langle \frac{|\mathbf{G}_r|^2}{2\eta P_{rad}} \right\rangle, \quad (B12b)$$

$$= \frac{8R_{ar} e_{rad}}{2\eta} \left(\frac{\lambda}{r_o} \right)^2 \oint \frac{|\mathbf{G}_r|^2}{2\eta P_{rad}} \frac{d\Omega}{4\pi}, \quad (B12c)$$

$$= \frac{8R_{ar} e_{rad}}{4\pi 2\eta} \left(\frac{\lambda}{r_o} \right)^2, \quad (B12d)$$

where we have used the assumption that the AoA of the scattered waves is isotropically distributed since the scatterers are uniformly distributed within the spherical scattering volume.

For the second ensemble average in (B6) and by using (6b) we straightforwardly obtain that

$$\left\langle \frac{1}{\rho_n^2} \right\rangle = \int_0^{R_s} \frac{1}{\rho^2} \frac{3\rho^2}{R_s^3} d\rho = \frac{3}{R_s^2}. \quad (\text{B13})$$

Combining (B9)–(B13) into (B6) provides the result in (22).

Data Availability Statement

The data have been deposited in a public accessible domain (https://figshare.com/articles/Data_for_AGU_Radio_Science_paper_Semi-analytical_model_of_the_Rician_K-factor/11907735).

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