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Primary Thermometry of Propagating Microwaves in the Quantum Regime

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The ability to control and measure the temperature of propagating microwave modes down to very low temperatures is indispensable for quantum information processing and may open opportunities for studies of heat transport at the nanoscale, also in the quantum regime. Here, we propose and experimentally demonstrate primary thermometry of propagating microwaves using a transmon-type superconducting circuit. Our device operates continuously, with a sensitivity down to 4×10^{-4} photons/ $\sqrt{\text{Hz}}$ and a bandwidth of 40 MHz. We measure the thermal occupation of the modes of a highly attenuated coaxial cable in a range of 0.001 to 0.4 thermal photons, corresponding to a temperature range from 35 mK to 210 mK at a frequency around 5 GHz. To increase the radiation temperature in a controlled fashion, we either inject calibrated, wideband digital noise, or heat the device and its environment. This thermometry scheme can find applications in benchmarking and characterization of cryogenic microwave setups, temperature measurements in hybrid quantum systems, and quantum thermodynamics.

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I. INTRODUCTION

Propagating modes of microwave waveguides play a key role in quantum information processing with superconducting circuits, connecting the quantum processor with the classical electronics controlling it [1]. Thermalization of these modes to the lowest achievable temperature is essential to limit unwanted decoherence of the quantum bits (qubits). At the same time, superconducting circuits are considered as a viable platform for thermodynamics experiments in the quantum regime [2–8]. In a prototypical such experiment, a quantum working medium, consisting, for example, of a small ensemble of superconducting artificial atoms, exchanges energy with one or more thermal reservoirs, or heat baths. These baths are often taken to be macroscopic (in the sense of fast-decaying correlations) and at thermal equilibrium, and are usually invoked to describe the operation of quantum heat engines and refrigerators. In this thermodynamic context, microwave waveguides, hosting a continuum of

modes with an Ohmic spectral density and smoothly interfacing with superconducting circuits, are natural candidates for realizing heat baths. Indeed, their use as (ideally) zero-temperature reservoirs has been pioneered in quantum state preparation and stabilization protocols based on dissipation engineering [9,10].

For these and other applications, a fast and accurate estimation of the thermal occupation of propagating microwave modes is highly desirable. An established method to obtain this estimate at steady state [11–18] relies on Ramsey measurements of the dephasing time of a qubit coupled to a cavity in the dispersive limit of circuit quantum electrodynamics. In this setting, the qubit dephasing rate Γ_ϕ depends linearly on the average thermal occupation of the cavity, due to the statistics of thermal photon shot noise in the quantum regime [15,19]. Based on an averaged measurement of a pulse sequence with a repetition time of the order of $1/\Gamma_\phi$ ($3 \mu\text{s}$ in Ref. [18]), this method is not compatible with continuous operation nor with single-shot readout of the thermal occupation. But the ability to track temperature changes in real time, with ns temporal resolution, is required to explore thermal dynamics under nonequilibrium conditions and to access thermodynamic quantities such as thermal relaxation rates, heat capacity, and temperature fluctuations in small systems [20,21]. In the context of thermodynamics, quantum-limited radiative heating and cooling mediated by microwave photons have been demonstrated [18,22–24]. In a

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series of recent experiments [4,6,25], the thermal photon occupation of microwave resonators was controlled and measured with the help of embedded mesoscopic metallic resistors acting as heat reservoirs for the confined microwave modes. Finally, efficient detectors of single propagating microwave photons have recently been demonstrated [26–30], which could, in principle, be used to determine the thermal photon occupation, albeit with a limited bandwidth and gated operation.

Here, we present the concept and experimental realization of a radiation-field thermometer for propagating fields, based on the coherent scattering of an artificial atom, which we refer to as a “quantum emitter,” strongly coupled to the end of a waveguide [31]. At vanishingly small power, zero temperature, and in the absence of additional dephasing channels, the scattering of a coherent tone at the emitter frequency is fully coherent. Thermal photons in the waveguide reduce the coherence of the process, leading to incoherent scattering and a detectable drop in reflectance. This drop is converted into thermal occupation by a simple algebraic expression involving device parameters that can be independently measured. This thermometry scheme is therefore primary, in the sense that it does not need to be calibrated against another thermometer [32].

We demonstrate this concept, which is otherwise general, using a transmon-type superconducting circuit [33] as the emitter. By realizing a large coupling between the transmon and the microwave waveguide to be measured, we minimize the relative impact of intrinsic decoherence mechanisms on the temperature readout. At the same time, we ensure that the transmon is in thermal equilibrium with the modes of the waveguide, as opposed to the uncontrolled environment that limits its intrinsic coherence time and would otherwise determine its steady-state thermal occupation [34,35]. We probe the response of the thermometer while increasing the radiation temperature in a controlled fashion. To do so, we first inject calibrated, wideband digital noise into the waveguide, a procedure that selectively targets the modes whose temperature is measured. Alternatively, we increase the temperature of the base plate of our refrigerator, which heats the waveguide modes but also the thermometer itself and its environment.

II. RESULTS

A. Concept, sample, and characterization

We implement the radiation-field thermometer as a superconducting, frequency-tunable, transmon-type artificial atom [33,36] coupled to the end of a coplanar microwave waveguide [scheme in Fig. 1(a) and micrograph in Fig. 1(b)]. The frequency of the transmon is tuned by the magnetic flux threading its superconducting quantum interference device (SQUID) loop, which we control by applying a dc current to an on-chip flux line. We operate the transmon at its highest fundamental frequency

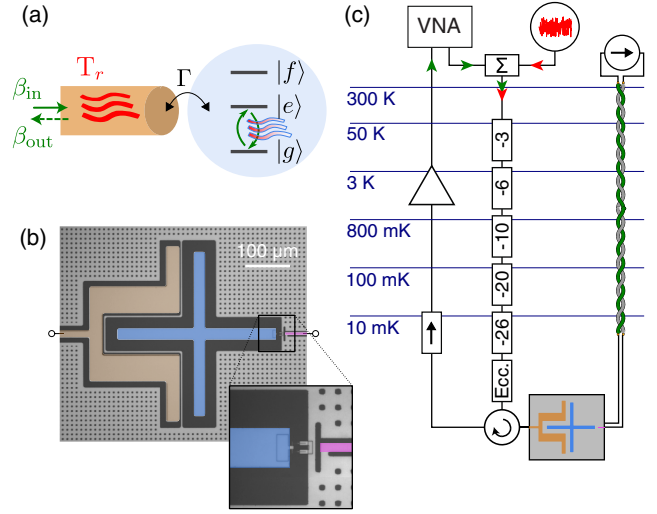


FIG. 1. Primary thermometry of propagating microwaves. (a) Concept: A ladder-type emitter is strongly coupled (with rate Γ) to the end of a waveguide. We monitor the scattering of a weak coherent tone, β_{in} (green straight arrow), resonant with the ground-to-first-excited-state transition of the emitter. Thermal photons in the waveguide at temperature T_r (wavy red lines) disturb the coherent oscillations of the emitter, leading to a decrease in the amplitude of the coherently scattered signal, β_{out} (green dashed arrow). (b) False-color micrograph of the superconducting circuit realizing the setting in panel (a): A transmon consisting of a superconducting island (blue) shunted by a superconducting quantum interference device (SQUID) is capacitively coupled to a coplanar waveguide (orange) and inductively coupled to a flux line (purple). The inset shows a close-up of the SQUID and the flux line. (c) Simplified scheme of the experimental setup (see text for details and Appendix A for the full wiring diagram).

$\omega_{ge}/2\pi = 5.332\text{GHz}$, commonly referred to as a “sweet spot,” to minimize flux-noise-induced dephasing. From single-tone spectroscopy (see below), we estimate the anharmonicity, $\alpha/2\pi = -217\text{MHz}$, and linewidth, $\Gamma/2\pi = 38\text{MHz}$, the latter dominated by the coupling to the waveguide. We measure the coherent scattering coefficient at the waveguide input with a vector network analyzer (VNA) in a configuration comprising a highly attenuated input line, an Eccosorb filter, a circulator, a chain of isolators, and a cryogenic high-mobility electron transistor (HEMT) amplifier [Fig. 1(c); see Appendix A for a full wiring diagram].

To increase the radiation-field temperature, we synthesize noise in the frequency band of interest [37]. All measurements are performed in a dilution refrigerator with a base temperature below 9 mK. To control the base temperature, we apply a current to heat a resistor anchored to the base plate. We characterize our sample by reflection spectroscopy at varying input powers P_{in} . To set the response of the transmon apart from the frequency-dependent transfer function of the input and output lines, all spectroscopy traces are referenced to a configuration in which the

transmon transitions are detuned at least 1 GHz below the frequency band of interest. We have also tested a high-power trace that fully saturates the transmon as a reference. These two procedures give equivalent results for input powers $P_{\text{in}} \geq 0$ dBm, implying, in particular, that our amplification chain is negligibly compressed at this power level. The high-power subtraction scheme can be conveniently used if a fixed-frequency transmon is used as the thermometer. With this calibration in place, we expect the most important source of inaccuracy to be related to imperfections in the circulator used to route the signals between the sample and our input and output lines. This issue is discussed in more detail in Appendix F.

At low values of P_{in} , the transmon is only weakly excited. Then, coherent scattering dominates, and the measured response is similar to that of a harmonic oscillator over-coupled to a transmission line. When sweeping the drive frequency across the resonance, the reflection coefficient shows a weak response in the amplitude [Fig. 2(a), bottom traces] and a full (180-degree) phase shift [Fig. 2(b)]. Increasing P_{in} increases the fraction of incoherent scattering from the transmon, resulting in a dip in the amplitude. As soon as incoherent scattering dominates over coherent scattering, the phase swing also starts to decrease. Eventually, the reflection coefficient at the fundamental resonance approaches unity as the emitter becomes saturated. In this high-power regime, however, higher-order transitions become observable as additional amplitude dips appearing at red-detuned frequencies. In particular, we clearly resolve the two-photon transition between the ground and second excited state, $\omega_{gf}/2$, and the three-photon transition between the ground and the third excited state, $\omega_{gh}/3$, detuned by $\alpha/2$ and α from the fundamental transition, respectively. We note that the visibility of these higher-order transitions is enhanced by the larger ratio between linewidth and anharmonicity, $\Gamma/|\alpha| = 0.18$, compared to previous work [31].

We model the response of the system by a master equation and input-output theory, taking up to four levels of the transmon into account (for more details on the simplifying assumptions, we refer to Appendix D). A global fit of our model to the spectroscopy data [Figs. 2(a) and 2(b), solid lines] presents an excellent agreement across a power range of 4 orders of magnitude. The inclusion of the fourth level is necessary to describe the third-order transition $\omega_{gh}/3$, the agreement otherwise being excellent also for a three-level model. From the global fit, we extract the values of ω_{ge} , Γ , α , as well as the thermal occupation n_r (see below), and the total line attenuation A from room temperature to the sample. Using the latter quantity, we can convert the input power P_{in} into a drive rate Ω via the relation

$$\Omega = 2\sqrt{A\Gamma P_{\text{in}}/\hbar\omega_{ge}}. \quad (1)$$

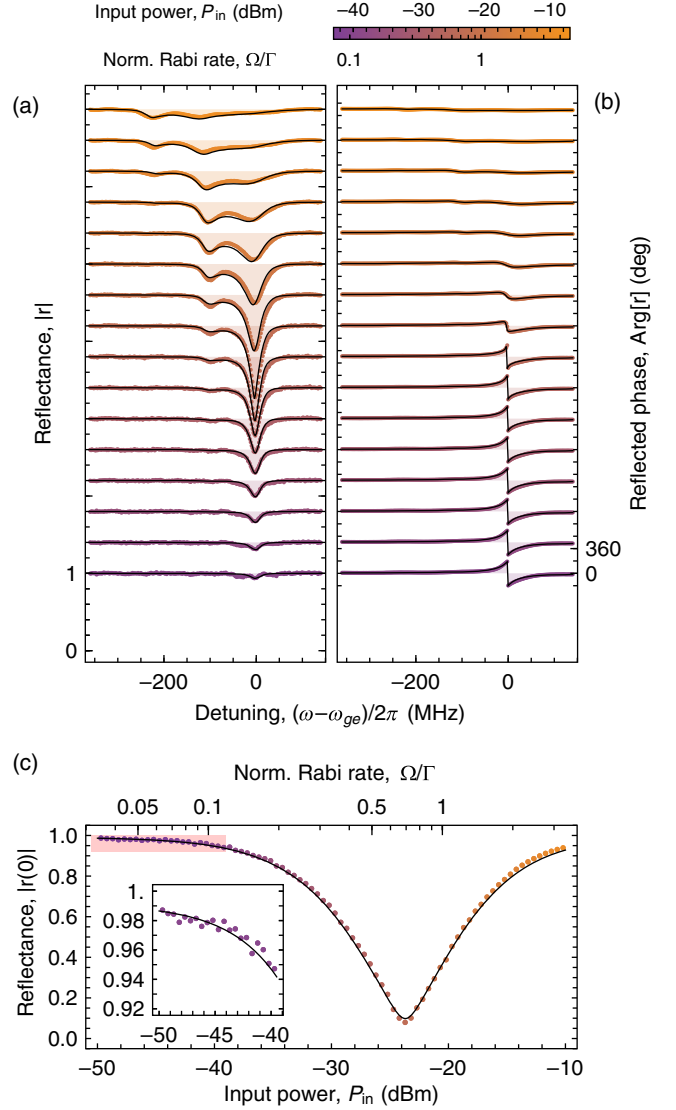


FIG. 2. Single-tone power spectroscopy. (a) Amplitude and (b) phase of the reflection coefficient versus drive detuning at selected input powers P_{in} in the range -39 to -9 dBm (colored dots). The traces are vertically offset by 0.4 (450 degrees) for the amplitude (phase). Solid lines show a global fit of a model to all traces (see text for details), from which sample parameters and total line attenuation are extracted. The shaded regions indicate deviations of the reflection coefficients from unit amplitude and zero phase. (c) Reflectance at resonance, $|r(0)|$, versus input power: measured values (dots) and theory (solid line). Inset: close-up of the shaded region in the main panel.

B. Thermometry concept

We now focus our attention on the power dependence of the magnitude of the reflection coefficient at resonance, $|r(0)|$ [Fig. 2(c)]. The observed V-shaped curve arises from the coherent interference between the radiation scattered by the emitter and that reflected by the open end of the waveguide, which carry opposite phase [38,39]. Note that a dip in the magnitude is not associated with a decrease in the

total reflected power but only with the coherent part of it; in our case, we estimate (based on the coupling rates given below) that over 99.99% of the power is always reflected. The measured $|r(0)|$ reaches a minimum of approximately 0.1 when the ratio of the drive rate over the linewidth is about $\Omega/\Gamma \approx 1/\sqrt{2}$. For a pure two-level system, the coherent reflection at resonance would vanish at this drive rate. For a transmon, complete destructive interference (cancellation) can still be attained, but the drive parameters at which this happens are affected by the presence of the third level. In particular, full cancellation is expected at a frequency detuned by $\Gamma^2/2\alpha \approx -3$ MHz (to first order in the ratio $\Gamma/|\alpha|$), which explains why the cancellation exhibited by the dip in Fig. 2(c) is only partial.

In the low-power limit $\Omega \ll \Gamma$, $|r(0)|$ approaches the asymptotic value 0.988, deviating from unity by 0.012 [Fig. 2(c), inset]. To explain this drop in reflectance, we consider three possible mechanisms: (i) decay to modes other than the waveguide, at the (nonradiative) rate Γ_{nr} , (ii) pure dephasing, at rate Γ_{ϕ} , and (iii) thermal occupation in the waveguide, n_r . We calculate the first-order contributions of these mechanisms to the reflection coefficient to be

$$r(0) = -1 + \frac{12}{1 + 3i\Gamma/2|\alpha|} n_r + 4 \frac{\Gamma_{\phi}}{\Gamma} + 2 \frac{\Gamma_{\text{nr}}}{\Gamma} + \frac{4(\Omega/\Gamma)^2}{1 + i\Gamma/|\alpha|}. \quad (2)$$

From Eq. (2), we notice that the impact of decoherence mechanisms is largely mitigated by our design choice of a large coupling to the waveguide. At the same time, the finite $\Gamma/|\alpha|$ ratio renormalizes the conversion factor linking reflection coefficient to thermal occupation. In the limit $\Gamma/|\alpha| \rightarrow 0$, the thermal occupation is related to the measured quantity r by an algebraic expression involving only numerical constants. Equation (2) also gives the first correction to the reflection coefficient due to finite input power (saturation), which is of second order in the ratio Ω/Γ .

Based on the estimates given in Sec. II E, we argue that the observed drop is most likely due to thermal occupation in the waveguide, $n_r = (1.0 \pm 0.3) \times 10^{-3}$, corresponding to an effective photon temperature $T_r = 37$ mK. To gain more confidence in the validity of this analysis, we have performed the measurements with added noise, reported below. For comparison, we estimate the expected temperature of the waveguide in the ideal case based on the attenuation configuration of the line [1], assuming perfect thermalization of the components at their stages (Appendix A), and find $T_r^{\text{est}} = 27$ mK (corresponding to $n_r^{\text{est}} = 8 \times 10^{-5}$). The measured radiation temperature is thus higher than what would be expected for an ideal chain of attenuators. This amount of excess thermal radiation is comparable to what is reported in other studies, including

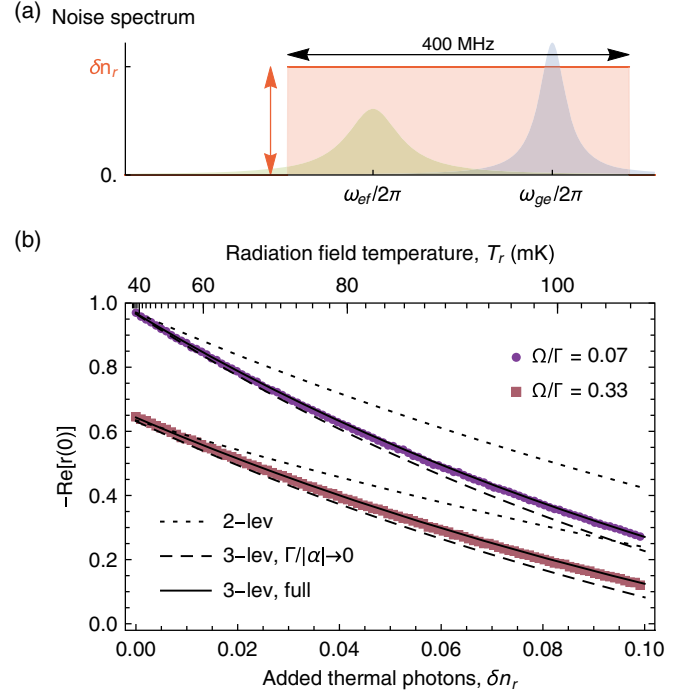


FIG. 3. Radiation-field thermometry with artificial white noise. (a) Sketch of the power spectral density of the applied noise (solid red line), with the relevant transmon transitions indicated on the frequency axis. The noise is white over a frequency band of 400 MHz and has a calibrated spectral density δn_r . Blue and green shades indicate the spectral densities of the transmon transitions, with a relative scaling reflecting their participation in the thermometry signal. (b) Measured real part of the reflection coefficient at resonance, $-\text{Re}[r(0)]$, at two selected drive strengths, $\Omega/\Gamma = 0.07$ and 0.33 , versus calibrated noise power expressed in added thermal photons, δn_r . The data (symbols) are directly compared to increasingly refined models, without free parameters: two-level theory (short dashes), three-level theory assuming a small linewidth-to-anharmonicity ratio, $\Gamma/|\alpha| \rightarrow 0$ (long dashes), and three-level theory taking the measured ratio $\Gamma/|\alpha| = 0.18$ into account (solid line).

some in which active steps have been taken to improve the thermal anchoring of attenuators to the mixing chamber plate [16,17,40].

C. Thermometry with added noise

To confirm our ability to measure the temperature of the radiation field in the waveguide, we increase it in a controlled fashion by applying white noise of adjustable root-mean-square amplitude over a 400-MHz bandwidth comprising the first two transitions of the transmon [Fig. 3(a)]. We take into account the finite noise bandwidth, introducing a windowing coefficient $w_{\text{win}} = 0.89$, determined by the overlap between the noise spectral density and the linewidths of the g - e and e - f transitions of the transmon, with a relative weight given by the participation of these transitions to the expected response in reflection

[see Appendixes D and E]. Using the calibrated attenuation of the line from the spectroscopy data, as well as a room-temperature calibration of the noise power compared to the power of the coherent tone used for the spectroscopy, we determine the added thermal noise in photons, δn_r , as a linear function of the noise power.

We study the response of the real part of the reflection coefficient at resonance, $\text{Re}[r(0)]$, to the added thermal noise at low ($\Omega/\Gamma = 0.07$) and intermediate ($\Omega/\Gamma = 0.33$) drive powers [Fig. 3(b)]. For both drive powers, an increase in δn_r produces a drop in $-\text{Re}[r(0)]$. The slope of the curve, $\partial\text{Re}[r(0)]/\partial\delta n_r$, gives the responsivity of the thermometer as a function of the photon occupation and is larger for the low-power trace. We discuss the trade-off between power and responsivity in Sec. II F (see also Fig. 5).

Our model for the drop in $-\text{Re}[r(0)]$, based on the parameters extracted from spectroscopy, agrees well with the data at both powers [Fig. 3(b), solid lines]. In particular, a best fit of the linear slope of the low-power trace for $\delta n_r \ll 1$ agrees with the predicted one within 1%. This agreement confirms the validity of the calibration scheme that we used, based on acquiring a reference trace with the transmon detuned: A systematic error in the calibration would produce a different slope. Conversely, if this scheme is not available or cannot be trusted, data sets such as the ones in Fig. 3 can themselves serve as a calibration.

For comparison, we also show the model for a two-level system (short dashes), and for a three-level transmon in the limit $\Gamma/|\alpha| \rightarrow 0$ (long dashes). The comparison against a two-level system highlights the fact that the second excited state $|f\rangle$ contributes to the response even at the smallest measured photon numbers, for which we expect its steady-state population to be negligibly small, $P_f \approx 10^{-5}$. Indeed, noise spectroscopy measurements (see Appendix B) confirm that the thermometer responds to thermal photons at both the fundamental and the first-to-second-excited-state transition, in agreement with the model. Finally, our comparison highlights the necessity to consider the finite value of the $\Gamma/|\alpha|$ ratio to reproduce the observed response. Since the $\Gamma/|\alpha|$ ratio can be accurately determined from spectroscopy, however, this fact does not compromise the primary nature of the thermometer.

D. Thermometry at different system temperatures

We vary the temperature of the radiation field in another, independent way by heating the base plate of the dilution cryostat. Differently from the noise injection experiment, in this case, the full system is warmed up, including the modes of the waveguide, which we expect to thermalize via the attenuators anchored to the base plate, but also the environment in which the thermometer resides, and, in particular, any spurious baths to which the transmon may be coupled.

We adjust the heating power to the base plate of the cryostat in time steps of 3 hours, and monitor the response

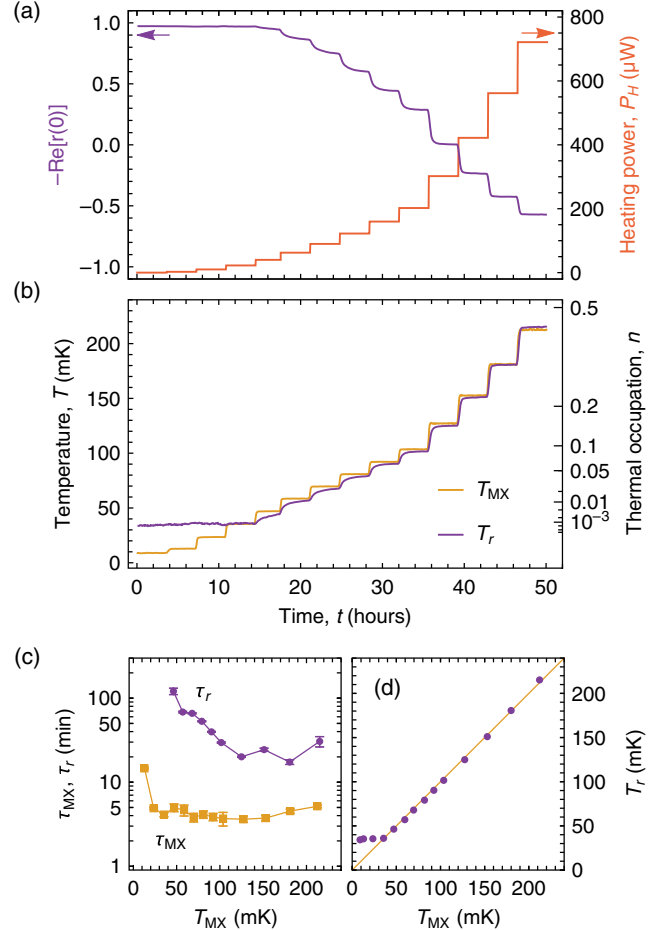


FIG. 4. Radiation-field thermometry while varying the temperature of the base plate. (a) Temporal profile of the heating power, P_H (right axis, red) used to vary the base-plate temperature T_{MX} , and corresponding temporal variation of the real part of the reflection coefficient (left axis, purple). (b) Corresponding base-plate temperature T_{MX} (yellow) and radiation-field temperature T_r (purple) versus time. (c) Thermal relaxation constants τ_{MX} (squares) and τ_r (circles) for T_{MX} and T_r , respectively, extracted from the data in panel (b) and plotted versus the steady-state T_{MX} . The solid lines are guides for the eye. (d) Steady-state values of T_r versus T_{MX} (circles); the solid line indicates $T_r = T_{MX}$.

of $-\text{Re}[r(0)]$ [Fig. 4(a)]. Consistently with the previous experiment, we observe that an increase in temperature results in a reduction of $-\text{Re}[r(0)]$. Compared to Fig. 3, here we study a larger variation in temperature and measure a correspondingly larger variation in $-\text{Re}[r(0)]$, in the range of 0.99 to -0.6 . Notice that the relation between $-\text{Re}[r(0)]$ and temperature is monotonic (and, therefore, single valued), even when the sign of $-\text{Re}[r(0)]$ changes from positive to negative.

Using the full theoretical expression for the reflection coefficient (Appendix D), we extract the thermal occupation, convert it into radiation temperature T_r , and compare it to the temperature of the base (mixing chamber) plate, T_{MX} , measured independently by a calibrated Ruthenium oxide

thermometer [Fig. 4(b)]. The measured T_r is insensitive to changes in T_{MX} as long as T_{MX} is below the saturated value of T_r . This insensitivity should not be interpreted as a limitation of the thermometer, whose ability to respond to small changes in noise photon number was demonstrated in Fig. 3. Instead, it can be explained by considering the exponential temperature dependence of the photonic occupation, according to the Bose-Einstein distribution. During the first temperature increments in T_{MX} , from 9 mK to 30 mK, the corresponding increase in thermal occupation is of the order of 2×10^{-4} , smaller than the residual thermal occupation measured at the base temperature. It is only after this temperature step that the increase in thermal occupation becomes significant, and T_r starts to follow T_{MX} . After a change in heating power, the adjustment of T_{MX} to its new steady-state value has an exponential tail with a time constant τ_{MX} between 4 and 5 minutes, which does not depend on temperature in the range considered [except for the first temperature step, for which $\tau_{MX} = 14$ min; Fig. 4(c)]. This timescale is related to the thermalization dynamics of the base plate as a whole. As temperature is increased, the linear increase in the heat capacity of the plate is compensated by a quadratic increase in the cooling power of the mixing chamber, resulting in a temperature-independent thermalization time.

By contrast, the adjustment of the radiation temperature T_r follows a much longer time constant τ_r , which is of the order of 2 hours at the lowest temperature and decreases by an order of magnitude as temperature is increased [Fig. 4(c)]. We ascribe this long timescale to a slow thermalization of the resistive section of the base-plate attenuators, whose voltage fluctuations set the temperature of the radiation field. At temperatures below 100 mK, the thermalization of these components generally proceeds via a cascade process, which involves electronic, phononic, and photonic channels [16,17,32,40]. The measured temperature dependence of τ_r may indicate a crossover between electron-dominated thermalization, with a thermal conductance proportional to temperature according to the Wiedemann-Franz law, and phonon-dominated thermalization, with a thermal conductance proportional to the fourth power of temperature for metals such as gold and copper [32].

We extrapolate the steady-state temperature at each step of the thermal sweep by fitting a decaying exponential to the tail of the relaxation data, and we plot the asymptotic value as a function of the steady-state temperature of the base plate [Fig. 4(d)]. The two values essentially agree over more than 2 orders of magnitude in thermal occupation number, from $n_r = 0.001$ to 0.4 (corresponding to a temperature range of 35 to 210 mK). This agreement indicates that a possible change in pure dephasing or other parameters, when varying the system temperature, does not affect the photon occupation number extracted from the scattering coefficient and thereby confirms the

validity of the thermometry scheme in the temperature range considered.

E. Impact of intrinsic decoherence channels

Based on measurements of transmon qubits fabricated on the same wafer [41], similar to those reported in Ref. [42], with identical geometry but no direct coupling to a waveguide, we estimate the intrinsic decay rate of the transmon $\Gamma_{nr}/2\pi < 4$ kHz ($T_1 > 40$ μ s) and its pure dephasing rate $\Gamma_\phi/2\pi < 2$ kHz ($T_2^* > 60$ μ s). These estimated rates are 10^4 times smaller than the decay rate into the waveguide; therefore, their direct measurement [43] is challenging. According to Eq. (2), we thus expect the combined pure dephasing and intrinsic decay mechanisms to cause a drop $|\delta r(0)| < 0.0004$, much smaller than what we observed even at the base temperature and in the absence of applied noise [Fig. 2(c)]. A change in either the radiation temperature of the waveguide (Sec. II C) or the temperature of the base plate (Sec. II D) could potentially increase these rates. However, in the temperature range considered, we expect their increase not to exceed the corresponding increase of the dephasing rate due to direct coupling to the waveguide. The latter will thus remain the dominant dephasing mechanism, as confirmed by the data in Fig. 4. Indeed, transmons typically show a very weak temperature dependence in T_1 up to around 150 mK, while the observed temperature dependence of the pure dephasing rate is usually due to photon shot noise in the readout resonator [17].

F. Sensitivity

We finally consider the sensitivity of this thermometry scheme. This figure is typically expressed as a noise equivalent temperature (NET), in units of K/ $\sqrt{\text{Hz}}$. However, given that the response of our detector is directly proportional to the thermal occupation n_r , and that the relation between n_r and T_r is strongly nonlinear in the deep quantum regime, $n_r \ll 1$, we prefer to provide this figure in noise equivalent thermal photons (NETP), which we calculate as

$$\text{NETP} = |\mathcal{R}|^{-1} \frac{\delta\beta_{\text{out}}}{\beta_{\text{in}}}, \quad (3)$$

where $\mathcal{R} = (\partial r / \partial n_r)$ is the responsivity of the reflection coefficient to changes in the thermal photon number, β_{in} is the incident coherent photon flux, and $\delta\beta_{\text{out}}$ is the noise in the detection chain. The latter can be expressed as $\delta\beta_{\text{out}} = 1/\sqrt{2\eta}$, where the factor $1/\sqrt{2}$ is due to quantum vacuum fluctuations and η is the quantum efficiency of the amplification chain [44]. As captured by Eq. (3), the optimum sensitivity is obtained as a trade-off between higher responsivity, obtained at lower drive powers, and a higher signal-to-noise ratio, obtained at higher drive powers (Fig. 5). In the limit $n_r \rightarrow 0$, the optimum drive rate is found to be $\Omega/\Gamma \approx 0.42$. The price to pay for an increased sensitivity

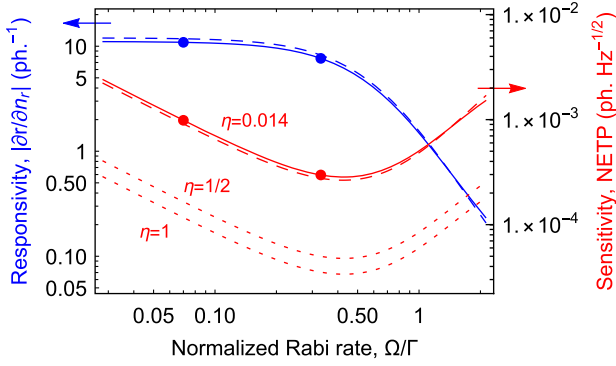


FIG. 5. Calculated photon number responsivity $|\partial r/\partial n|$ (left axis) and sensitivity NETP (in photons per square root bandwidth, right axis) versus normalized Rabi rate Ω/Γ in the low-occupation limit $n \rightarrow 0$ and for the measured sample and setup parameters (solid lines). Dashed lines are calculated in the limit $\Gamma/|\alpha| \rightarrow 0$ (see text for details). The dashed lines are the projected sensitivities using the same sample and an amplification chain with efficiencies $\eta = 1/2$ and $\eta = 1$. Thick dots indicate the responsivity and sensitivity measured with our setup ($\eta = 0.14$) at the two driving powers used in Fig. 3.

is that the responsivity depends on the normalized Rabi rate Ω/Γ . However, since the latter can be easily calibrated (see Fig. 2), this is not a major limitation. A large radiative linewidth Γ is generally beneficial for the sensitivity because it increases the photon flux that can be scattered by the transmon while keeping the ratio Ω/Γ constant and therefore improves the signal-to-noise ratio.

In our experiment, we evaluate the sensitivity by measuring the standard deviation of repeated measurements at various drive rates and measurement bandwidths, extract the signal-to-noise ratio, and multiply it by the theoretical responsivity. Alternatively, we first measure the quantum efficiency of our amplification chain by comparing the power spectrum of the resonantly driven transmon at saturation with the noise level, and then use the theoretical expression. We measure sensitivities of the order of 1×10^{-3} photons/ $\sqrt{\text{Hz}}$ at low drive rates and 4×10^{-4} photons/ $\sqrt{\text{Hz}}$ close to the optimum drive rate (Fig. 5, large dots). The best sensitivity we measured is limited by our amplification chain, with an added noise of 35 photons and corresponding quantum efficiency $\eta = 0.014$. For an amplification chain working close to the standard quantum limit $\eta = 0.5$, which has been reached and even surpassed using phase-sensitive Josephson parametric amplifiers [45,46], this number could be further improved by 1 order of magnitude (dashed line in Fig. 5). Finally, we notice that the presented device can also be operated as a narrow-band bolometer. In the current measurement setup, the corresponding noise-equivalent power (NEP) is of the order of

$$\text{NEP} \approx \hbar\omega_{ge}\Gamma \times \text{NETP} \approx 400 \text{ zW}/\sqrt{\text{Hz}}. \quad (4)$$

For comparison, NEPs in the range of a few hundred down to a few $\text{zW}/\sqrt{\text{Hz}}$ have been reported for nanobolometers based on metallic absorbers operating in the microwave frequency range [47,48].

III. DISCUSSION

In summary, we have demonstrated that a single quantum emitter strongly coupled to the end of a waveguide can be used for sensitive measurement of the thermal occupation of the waveguide, using simple continuous-wave, single-tone spectroscopy. By applying synthesized noise of controlled spectral content, we explored the response of the thermometer to a frequency-dependent thermal occupation. Thanks to a large coupling rate of the transmon to the waveguide, we minimized the effect of the intrinsic decoherence mechanisms of the emitter on the temperature readout (for the numbers given in the text, their contribution to the measured thermal occupation is of the order of 1×10^{-4} , 1 order of magnitude smaller than the lowest measured value).

The presented device can probe the thermal occupation of attenuated waveguides used to control quantum information processors, in a range relevant for state-of-the-art applications. In conjunction with a cryogenic single-pole, multiple-throw microwave switch [49], it can be used to directly benchmark the performance of filtering, attenuation, and thermalization layouts. At the same time, it holds unique features that may enable a novel range of experiments in mesoscopic calorimetry and heat transport, as well as stochastic and quantum thermodynamics. First, it combines continuous operation, fast response in time (< 10 ns), and high sensitivity. It is also a primary thermometer, which provides accuracy without reliance on external calibrations. Finally, its detection frequency is tunable, so it can be operated as an on-chip “spectrum analyzer” scanning a GHz-wide frequency band. Thanks to these features, it can be utilized to monitor, in real time, the temperature of a radiating body such as a mesoscopic electron reservoir, to which it can be coupled via a matching circuit. This reservoir could, in turn, be the absorber of a nanocalorimeter or nanobolometer operated as a single-photon detector in a higher frequency band. In the context of quantum thermodynamics, it will make it possible to investigate steady-state properties and dynamics of quantum heat engines and refrigerators, including instantaneous heat flows and time-resolved photon-photon correlations.

In future realizations, the transmon qubit may be replaced by Josephson-based artificial atoms with larger anharmonicities [14] and/or different level structures, possibly also in the ultrastrong coupling regime [50]. Nonsuperconducting emitters could also be considered, such as semiconductor quantum dots [51].

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APPENDIX A: EXPERIMENTAL DETAILS

1. Setup

The radiation-field thermometer is mounted at the mixing chamber stage of a dilution refrigerator (see Fig. 6) and is enclosed in a nonmagnetic environment, shielded by a μ -metal shield and an absorber shield. At room temperature, digital noise is synthesized by an arbitrary-waveform generator (AWG), mixed with a local oscillator using an in-phase-quadrature mixer, combined with a coherent probe tone from the VNA, and fed to a highly attenuated input line that includes a low-pass filter and an Eccosorb filter at the base temperature. A cryogenic circulator is used to route the signal reflected from the sample to the output line, which has a cryogenic high-mobility electron-transistor (HEMT) amplifier mounted at the 3-K stage. A high-pass filter, a low-pass filter, and four isolators are used to isolate the sample from radiation emitted by the HEMT. A dc current is fed to the flux line of the thermometer via a twisted pair of low-ohmic cables, interrupted at the 3-K stage by a low-pass filter.

To increase the temperature of the base plate of the dilution cryostat and obtain the results reported in Fig. 4, we apply a current to heat a resistor anchored to the base plate. Based on finite-element simulations taking into account the relative positioning of the different elements on the base plate (Fig. 7), we observe that (i) the steady-state temperature difference across the base plate is well below 1 mK for all experimental points in Fig. 4, and (ii) upon a sudden change in heating power, different parts of the base plate follow the same temporal evolution within the same accuracy. We thus conclude that the exact positioning of the different elements on the base plate does not significantly affect the quantities plotted in Fig. 4.

2. Noise generation

To generate noise with arbitrary spectral properties, we start from a string of random real numbers sampled from a normal distribution with zero mean and unit variance (white noise). We (unessentially) take the discrete

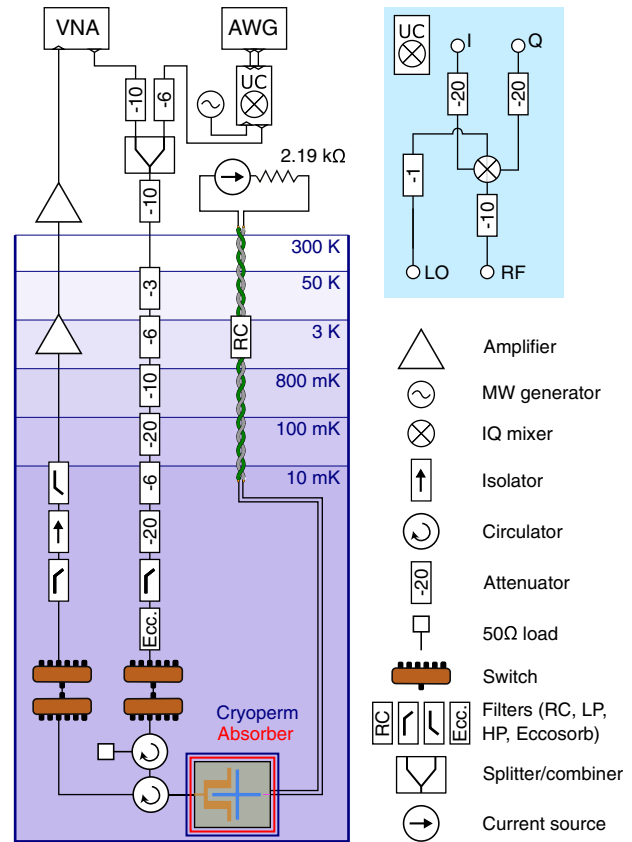


FIG. 6. Full wiring diagram for the experiment. MW is for microwave, LP for low pass, and HP for high pass.

Fourier transform of this signal and apply a filter centered at the intermediate frequency $\omega_{IF}/2\pi = 220$ MHz, with unit amplitude and the desired spectral profile. The filter only has support at positive frequencies. We then invert the Fourier transform and send the real and imaginary parts of the complex signal to the in-phase and quadrature ports of the up-conversion (UC) mixer. With this procedure, the noise is up-converted to a single sideband [37].

To compensate for frequency-dependent conversion loss in the mixer, we generate white noise across the frequency band of interest, measure its spectral density at room

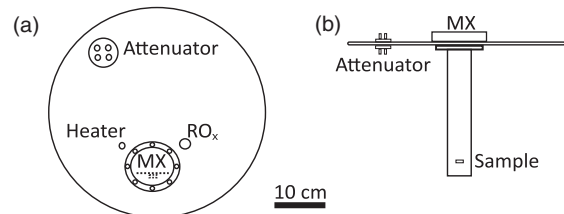


FIG. 7. Schematic representation of the base plate of the dilution refrigerator [(a) top view and (b) side view], indicating the positioning of the mixing chamber (MX), the ruthenium-oxide thermometer (RO_x), the thermal anchoring point of the attenuator, and the sample.

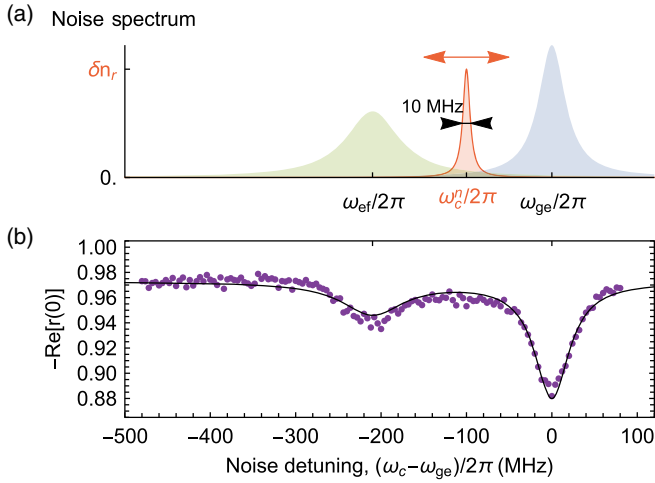


FIG. 8. Noise spectroscopy with Lorentzian noise. (a) Power spectral density of the applied noise, a 10-MHz Lorentzian with fixed amplitude, and varying center frequency $\omega_c/2\pi$. (b) Real part of the reflection coefficient at resonance, $-\text{Re}[r(0)]$, versus noise detuning from the fundamental transition (dots), and corresponding theory prediction (solid line) based on the same parameters as in Fig. 3.

temperature with a spectrum analyzer, and use the result to calculate a frequency-dependent transfer function for the mixer. In subsequent experiments, we apply the transfer function to the digital filter that determines the noise properties so that the spectral density of the up-converted noise, measured at room temperature, matches the intended one.

APPENDIX B: NOISE SPECTROSCOPY

To determine the relative participation of noise applied at different frequencies to the dip in reflection, we apply Lorentzian noise with varying center frequency and a linewidth of 10 MHz (Fig. 8). As expected, we obtain the strongest response when the applied noise is resonant with the g - e transition. However, we also observe a sizable dip at the e - f resonance. Indeed, a careful theoretical analysis assigning different thermal occupations to the radiation field at the two transitions (see Appendix D 2) reveals that both transitions participate in dephasing, with a relative strength of 2:1 (in the linear-response limit, $n_r \ll 1$). This ratio has a simple physical explanation, namely, that thermal photons at the g - e transition induce both population change and dephasing, while those at the e - f induce only dephasing on the g - e transition (the state $|e\rangle$ is virtually unpopulated when both n_r and Ω/Γ are small).

APPENDIX C: RESPONSE TO A FAST CHANGE IN TEMPERATURE

To investigate the temporal response of the thermometer to a fast change in temperature, we modify the room-temperature part of the experimental setup (Fig. 9).

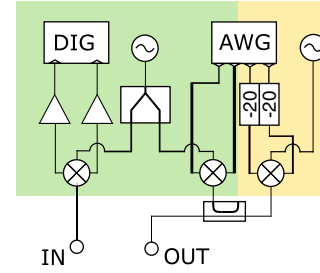


FIG. 9. Room-temperature setup for the measurements in Appendix C. DIG is for digitizer. Circuit symbols are defined in Fig. 6.

The arbitrary waveform generator (1 GSa/s sample rate) synthesizes both a digital noise pulse and a coherent pulse, which are separately up-converted and then combined and fed to the input line of the cryostat. The signal from the output line is down-converted and recorded by a digitizer (500 MSa/s sample rate).

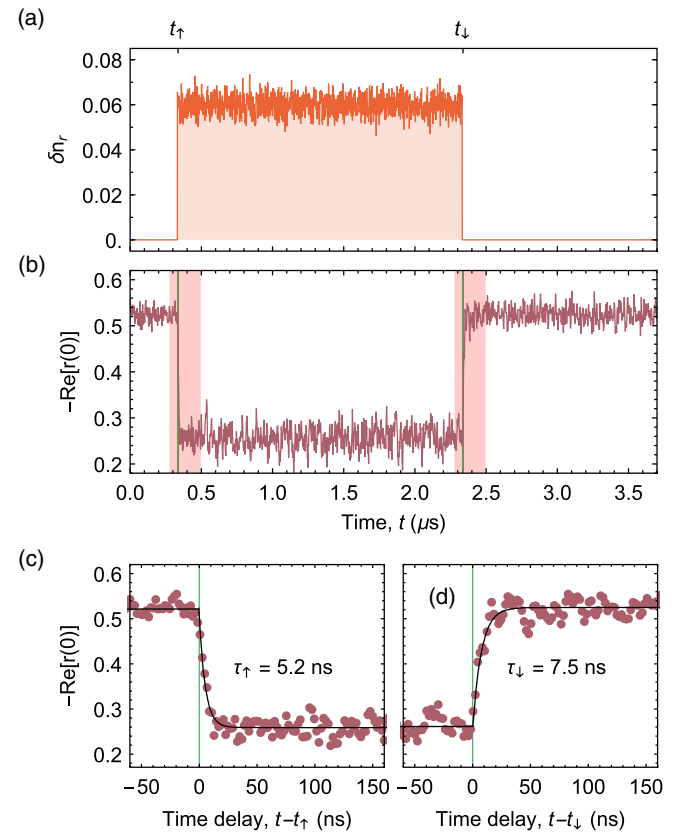


FIG. 10. Temporal response of the thermometer. (a) Photon occupation number of the applied noise pulse, δn_r , vs time, calibrated and averaged over noise realizations. (b) Measured real part of the reflection coefficient at resonance, $-\text{Re}[r(0)]$, vs time. Green vertical lines denote the start and end times of the noise pulse (t_\uparrow and t_\downarrow , respectively). (c,d) Close-up of the shaded regions in panel (b) at the leading and trailing edges of the thermometer response (dots). The solid red lines are fits of a single exponential function to the data, giving a ring-up time $\tau_\uparrow = 5.2$ ns and a ring-down time $\tau_\downarrow = 7.5$ ns.

We drive the thermometer with a 8- μ s-long coherent pulse at the Rabi rate $\Omega/\Gamma \approx 0.35$. Two microseconds after the beginning of the coherent pulse, we inject a noise pulse with a spectral content centered between the emitter's first and second transition frequencies, with a frequency span of 400 MHz, a duration of 2 μ s, and a calibrated photon number of $n \approx 0.06$ [Fig. 10(a)]. The recorded real part of the reflected signal responds to the applied noise pulse [Fig. 10(b)]. By fitting single exponentials to the leading and trailing edges of the response, we find the settling times $\tau_{\uparrow} = 5.2$ ns for the leading edge and $\tau_{\downarrow} = 7.5$ ns for the trailing edge, respectively [Figs. 10(c) and 10(d)]. For comparison, similar fits to the numerically simulated response of the thermometer, based on the estimated parameters, give $\tau_{\uparrow} = 6.9$ ns and $\tau_{\downarrow} = 8.2$ ns. We understand these settling times as determined by the dephasing rate of the g - e transition of the qubit, which is probed by the coherent tone. According to this reasoning, a simple estimate for the temporal resolution of the thermometer is the inverse of the dephasing rate, $\tilde{\Gamma}_{\phi} = (1 + 2n_r)\Gamma/2$. The dependence on n_r explains why the thermometer responds faster when settling to a higher photon temperature. In addition, a finite drive rate contributes to the dephasing and hence makes the response faster. Further theoretical insight into this dynamics is provided in Appendix D 5.

APPENDIX D: RADIATION-FIELD THERMOMETER MODEL

1. Master equation and steady-state solution

In a frame rotating at the drive frequency ω_d and using a rotating-wave approximation, we describe the driven transmon by the Hamiltonian

$$\hat{H} = -\delta \hat{b}^\dagger \hat{b} + \frac{\alpha}{2} \hat{b}^\dagger \hat{b}^\dagger \hat{b} \hat{b} + i \frac{\Omega}{2} (\hat{b} - \hat{b}^\dagger), \quad (\text{D1})$$

where \hat{b} is an annihilation operator, $\delta = \omega_d - \omega_{ge}$ is the drive detuning from the fundamental resonance, α is the transmon anharmonicity ($\alpha < 0$), and Ω is the drive strength [33].

The coupling to the waveguide induces transitions between adjacent energy eigenstates of the transmon, described by lowering and raising operators $\sigma_-^j = |j\rangle\langle j+1|$ and $\sigma_+^j = |j+1\rangle\langle j|$ for the j th transition, respectively ($|j\rangle$ denotes the j th state). We consider frequency-dependent coupling strengths and thermal occupations, so the waveguide modes around the j th transition are coupled to the transmon with relative strength ξ_j and are characterized by a thermal occupation $n_{\text{th}}^{(j)}$. For our experiment, we assumed a constant density of states in the waveguide, so $\xi_j = \sqrt{j}$ due to the dipole matrix elements of the transmon [33]. We thus derive a master equation in a ‘‘local’’ Born-Markov approximation (around the frequency of each transition) [52]. The dissipative

interaction between the transmon and the waveguide is described by a Liouvillian superoperator \mathcal{L}_Γ , acting on the density matrix ρ in a Hilbert space truncated to the first N states:

$$\mathcal{L}_\Gamma \rho = \Gamma \sum_{l,m=1}^N \xi_l \xi_m [(1 + n_{\text{th}}^{(m)}) \mathcal{D}_{l,m}^-[\rho] + n_{\text{th}}^{(m)} \mathcal{D}_{l,m}^+[\rho]], \quad (\text{D2})$$

where Γ is the decay rate of the fundamental transition. We have introduced generalized dissipators

$$\mathcal{D}_{l,m}^\pm[\rho] = -\frac{1}{2}(\rho \sigma_{\mp}^m \sigma_{\pm}^l + \sigma_{\mp}^l \sigma_{\pm}^m \rho - \sigma_{\pm}^l \rho \sigma_{\mp}^m - \sigma_{\pm}^m \rho \sigma_{\mp}^l), \quad (\text{D3})$$

which describe excitation (decay) of the l th transition of the transmon, accompanied by absorption from (emission into) the waveguide of a photon with the energy of the m th transition. Terms with $l \neq m$ rotate at the frequency difference between the two transitions in the interaction picture. If the linewidths of the transitions are much smaller than the difference between their frequencies, then these terms can be neglected by invoking a rotating-wave approximation [39]. Here, however, because of the finite $\Gamma/|\alpha|$ ratio, these cross-terms introduce a correction, which we take into account. When terms with $m \neq n$ are neglected in Eq. (D2), we recover the more familiar expression

$$\mathcal{L}_\Gamma \hat{\rho}(t) = \Gamma \sum_{j=1}^N \xi_j^2 [(1 + n_{\text{th}}^{(j)}) \mathcal{D}[\sigma_-^j, \hat{\rho}(t)] + n_{\text{th}}^{(j)} \mathcal{D}[\sigma_+^j, \hat{\rho}(t)]], \quad (\text{D4})$$

with the dissipator

$$\mathcal{D}[A, B] = ABA^\dagger - \frac{1}{2}(A^\dagger AB - BA^\dagger A). \quad (\text{D5})$$

We model pure dephasing at a rate Γ_ϕ by adding the following Liouvillian to the master equation:

$$\mathcal{L}_{\Gamma_\phi} \hat{\rho}(t) = \Gamma_\phi \sum_{j=1}^N \mathcal{D}[|j\rangle\langle j|, \hat{\rho}(t)]. \quad (\text{D6})$$

Finally, we model nonradiative decay to an additional bath (taken at zero temperature for simplicity) at rate Γ_{nr} , by a Liouvillian $\mathcal{L}_{\Gamma_{\text{nr}}}$, which we obtain from Eq. (D2) with the replacements $\Gamma \rightarrow \Gamma_{\text{nr}}$ and $n_{\text{th}}^{(m)} \rightarrow 0$. Putting things together, the master equation reads

$$\dot{\rho}(t) = -\frac{i}{\hbar}[H, \rho(t)] + \mathcal{L}_\Gamma \rho(t) + \mathcal{L}_{\Gamma_\phi} \rho(t) + \mathcal{L}_{\Gamma_{\text{nr}}} \rho(t). \quad (\text{D7})$$

We obtain the steady-state density matrix by an analytical solution of the algebraic equation $\dot{\rho}(t) = 0$. From that

solution and using input-output theory, the reflection coefficient can be written as

$$r = 1 + \frac{2\Gamma}{\Omega} \sum_j \xi_j \rho_{j,j+1}. \quad (\text{D8})$$

2. Reflection coefficient in the small excitation limit

We take $N = 3$, which is fully appropriate to describe scattering when $\Omega \lesssim \Gamma$. We consider resonant scattering ($\delta = 0$) and make a first-order expansion in the small quantities n_r^{ge} , n_r^{ef} , Γ_ϕ/Γ , and Γ_{nr}/Γ , and a second-order expansion in the ratio Ω/Γ . We arrive at the following expression:

$$r(0) = -1 + \frac{8n_r^{ge} + 4n_r^{ef}}{1 + 3i\Gamma/2|\alpha|} + 4\frac{\Gamma_\phi}{\Gamma} + 2\frac{\Gamma_{nr}}{\Gamma} + \frac{4(\Omega/\Gamma)^2}{1 + i\Gamma/|\alpha|}. \quad (\text{D9})$$

Taking $n_r = n_r^{ge} = n_r^{ef}$ gives Eq. (2) in the main text.

3. Reflection coefficient for a two-level system

Solving the master equation for a two-level system results in the following expression for the reflection coefficient:

$$r(0)_{\text{TLS}} = -1 + 4\frac{2n_r + 2n_r^2 + (\Omega/\Gamma)^2}{1 + 4n_r + 4n_r^2 + 2(\Omega/\Gamma)^2}. \quad (\text{D10})$$

Notice that a two-level system is not equivalent to a three-level system in the limit $\Gamma/|\alpha| \rightarrow 0$ because of the effect of thermal photons at the first-to-second-excited-state transition. Equation (D10) is plotted as a dotted line in Fig. 3(b).

4. Sensitivity and responsivity

Taking the derivative of the reflection coefficient at resonance in the limits $\Gamma/|\alpha| \rightarrow 0$ and $n_r \ll 1$ with respect to n_r gives the following expression for the responsivity:

$$\mathcal{R} = \frac{2(6 + \Omega_r^2)}{(1 + 2\Omega_r^2)^2}, \quad (\text{D11})$$

where $\Omega_r = \Omega/\Gamma$. By inserting Eq. (D11) into Eq. (3), we obtain the sensitivity

$$\text{NETP} = \frac{(1 + 2\Omega_r^2)^2}{\sqrt{2\Gamma\eta}\Omega_r(6 + \Omega_r^2)}. \quad (\text{D12})$$

These expressions are plotted as dashed lines in Fig. 5.

5. Dynamics

To estimate the response of the thermometer in time, we solve its dynamics upon a sudden change in thermal

occupation n_r from an initial value n_0 to a different value n_1 . To do so, we solve the master equation (D7) with $n_r = n_1$, taking as the initial density matrix the steady-state solution of the same equation with $n_r = n_0$. We then calculate the time-dependent reflection coefficient according to Eq. (D8).

To gain analytical insight, we consider a resonantly driven, two-level system in the limits of small drive ($\Omega/\Gamma \ll 1$) and thermal occupation ($n_0, n_1 \ll 1$). (We also neglect non-radiative decay and pure dephasing.) The reflection coefficient is well approximated by the expression

$$r(\tau) = \bar{r}_1 + (\bar{r}_0 - \bar{r}_1)e^{-\tilde{\Gamma}_\phi\tau}(3 - e^{-\tilde{\Gamma}_\phi\tau})/2, \quad (\text{D13})$$

where \bar{r}_0 (\bar{r}_1) is the steady-state reflection coefficient at thermal occupation n_0 (n_1), and $\tilde{\Gamma}_\phi = (1 + 2n_1)\Gamma/2$ is the dephasing rate of the qubit. From Eq. (D13), we thus see that the thermometer responds to changes in thermal occupation of the waveguide with a time constant equal to its dephasing time, which is to be expected given that thermal dephasing is the enabling mechanism for thermometry.

Numerical simulations (not shown) indicate that the same time constant also limits the response when the third level of the transmon is included in the calculation. We explain this fact by considering that the dephasing rate at the e - f transition is twice as large as for the g - e transition, so thermal relaxation is still limited by the latter.

APPENDIX E: DATA ANALYSIS

1. Noise windowing

We introduce a weight function

$$w(\omega) = \frac{8}{12}f_L(\omega - \omega_{ge}, \Gamma) + \frac{4}{12}f_L(\omega - \omega_{ef}, 2\Gamma), \quad (\text{E1})$$

where $f_L(\omega, \Gamma)$ is a normalized Lorentzian of linewidth Γ . For a frequency-dependent noise profile $S(\omega)$, we calculate an effective added photon number as

$$\delta n_r^{\text{eff}} = \int d\omega w(\omega)S(\omega). \quad (\text{E2})$$

For a 400-MHz white noise of amplitude δn_r (Fig. 3), we find $\delta n_r^{\text{eff}} = \delta n_r w_{\text{win}}$, with $w_{\text{win}} = 0.89$.

2. Conversion between thermal occupation and temperature

If the waveguide is thermalized at a temperature T_r , the thermal occupation at a given frequency is given by the Bose distribution

$$n(\omega, T_r) = \frac{1}{\exp(\hbar\omega/k_B T_r) - 1}. \quad (\text{E3})$$

The effective thermal occupation sensed by the thermometer as it appears in Eq. (2), taking into account Eq. (D9), is given by

$$n_r(T_r) = \frac{2}{3}n(\omega_{ge}, T_r) + \frac{1}{3}n(\omega_{ef}, T_r). \quad (\text{E4})$$

To convert thermal occupation into temperature, we numerically invert Eq. (E4), which is a monotonic function of T_r .

3. Estimate of thermal occupation based on nominal attenuation

To estimate the thermal occupation of the waveguide, we model each attenuator as a beam-splitter combining the incoming signal with a thermal state with occupation $n(\omega, T_{i,\text{att}})$, corresponding to the temperature $T_{i,\text{att}}$ of the stage at which the attenuator resides. The thermal occupation $n_i(\omega)$ after the i th thermalization stage with attenuation A_i is thus given by [1]

$$n_i(\omega) = \frac{n_{i-1}(\omega)}{A_i} + \frac{A_i - 1}{A_i} n(\omega, T_{i,\text{att}}). \quad (\text{E5})$$

APPENDIX F: INFLUENCE OF AN IMPERFECT CIRCULATOR IN THE REFERENCED REFLECTION MEASUREMENT

As explained in the main text, we take advantage of the fact that we can “switch off” our emitter *in situ*, either by detuning its frequency outside of the band of interest or by saturating it with a strong coherent tone to obtain a calibration trace for our measurement chain. Using this trace as a reference in our reflection measurements, we effectively cancel out the frequency-dependent transfer function of the chain. However, this procedure does not account for interference effects that can be introduced by imperfections in the circulator used to route the signals from the input line to the device under test (DUT) and from the DUT to the output line. In this section, we model our measurement in the presence of an imperfect circulator and provide an estimate for the systematic error that an imperfect circulator introduces in our temperature measurements.

Because of the finite isolation of the circulator, part of the probe signal will leak directly from the input port (port 1 in the following) to the output port (port 3) and interfere with the signal that has followed the intended path towards the DUT (port 2), then to the DUT and back, and finally to the output port. We are interested in the relation between the reflection coefficient of the DUT, Γ_{DUT} , and the transmission coefficient \bar{t} measured across the network. Our configuration can be described as a three-port network with scattering parameters s_{ij} (the circulator), with one port connected to a load with reflection coefficient Γ_L , and the other two ports matched. A simple analysis of the associated signal flow diagram [53] gives

$$\bar{t} = AG \left(s_{31} + \frac{s_{21}\Gamma_L s_{32}}{1 - s_{22}\Gamma_L} \right), \quad (\text{F1})$$

where A and G stand for attenuation and gain before and after the circulator, respectively. We write the scattering matrix of a lossless, symmetric, imperfect circulation with isolation γ as

$$s_{ij} = \begin{pmatrix} -\gamma & \gamma & 1 - \gamma^2 \\ 1 - \gamma^2 & -\gamma & \gamma \\ \gamma & 1 - \gamma^2 & -\gamma \end{pmatrix}_{ij}. \quad (\text{F2})$$

In modeling the reflection coefficient of the load, we take into account electrical delay τ and a phase shift ϕ so that

$$\Gamma_L(\omega) = \Gamma_{\text{DUT}}(\omega) \exp(i\omega\tau + i\phi). \quad (\text{F3})$$

We note in passing that the effect of cable attenuation between the circulator and the sample, which we neglect in the following, can be modeled by adding a small imaginary part to the phase ϕ . Finally, to model the referenced reflection coefficient r_{refd} , we take the ratio between the expected transmission when $\Gamma_{\text{DUT}} = r_{\text{ideal}}$ (r_{ideal} being the theory prediction) and $\Gamma_{\text{DUT}} = 1$:

$$r_{\text{refd}} = \frac{\bar{t}(\Gamma_{\text{DUT}} = r_{\text{ideal}})}{\bar{t}(\Gamma_{\text{DUT}} = 1)}. \quad (\text{F4})$$

We now focus on the case of resonant reflection and small thermal occupation, for which $r_{\text{ideal}} \approx -1 + \delta_r$ and $\delta_r \approx 12n_r \ll 1$. A series expansion in the small parameters γ and δ_r thus gives, for the real part, imaginary part, and absolute value of r_{meas} ,

$$\text{Re}[r_{\text{refd}}] = r_{\text{ideal}} + 8\gamma^2 \sin^2(\omega\tau + \phi) + 2\gamma\delta_r \cos(\omega\tau + \phi), \quad (\text{F5})$$

$$\text{Im}[r_{\text{refd}}] = -4\gamma \sin(\omega\tau + \phi) + 4\gamma\delta_r \sin(\omega\tau + \phi), \quad (\text{F6})$$

$$|r_{\text{refd}}| = |r_{\text{ideal}}| - 2\gamma\delta_r \cos(\omega\tau + \phi). \quad (\text{F7})$$

Notice that the first correction is of first order in the small quantities for the imaginary part but only of second order for the real part and the absolute value. By realistically choosing $\gamma = 0.08$ (corresponding to 22-dB isolation) and $\delta_r = 0.06$ (or $n_r = 5 \times 10^{-3}$), the maximum error on the real part due to interference effects is 0.05 (or 4×10^{-3} in thermal occupation), while the maximum error on the absolute value is 0.01 (or 9×10^{-4} in thermal occupation).

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