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# Hyperparametric Oscillation via Bound States in the Continuum

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Optical hyperparametric oscillation based on the third-order nonlinearity is one of the most significant mechanisms to generate coherent electromagnetic radiation and produce quantum states of light. Advances in dispersion-engineered high- $Q$  microresonators allow for generating signal waves far from the pump and decrease the oscillation power threshold to submilliwatt levels. However, the pump-to-signal conversion efficiency and absolute signal power are low, fundamentally limited by parasitic mode competition and attainable cavity intrinsic  $Q$  to coupling  $Q$  ratio, i.e.,  $Q_i/Q_c$ . Here, we use Friedrich-Wintgen bound states in the continuum (BICs) to overcome the physical challenges in an integrated microresonator-waveguide system. As a result, on-chip coherent hyperparametric oscillation is generated in BICs with unprecedented conversion efficiency and absolute signal power. This work not only opens a path to generate high-power and efficient continuous-wave electromagnetic radiation in Kerr nonlinear media but also enhances the understanding of a microresonator-waveguide system—an elementary unit of modern photonics.

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Optical hyperparametric oscillation (H-OPO) emerges in a driven  $\chi^{(3)}$  nonlinear cavity as a result of modulation instability (MI) that amplifies vacuum photons. Two pump photons are converted into a pair of correlated photon pairs ( $2\hbar\omega_p \rightarrow \hbar\omega_s + \hbar\omega_i$ ) at new frequencies [Fig. 1(a)]. This elementary mechanism lies at the onset of microresonator frequency comb generation [1] and has served for generating coherent light sources [2–7] and quantum technologies [8–14]. High- $Q$  microresonators, either in whispering gallery mode [15,16], planar [17–24], or photonic crystal cavities [25], provide means to decrease the power oscillation threshold. With dispersion engineering, broadband H-OPO has been demonstrated [26–30].

A critical metric in any parametric oscillator is the conversion efficiency, i.e., the ratio of signal power compared to the pump. This metric is first limited by mode competition among different longitudinal modes in the cavity and nondegenerate four-wave mixing [31]. The gain required to sustain H-OPO originates from MI. For a fixed dispersion, the gain's peak and bandwidth are determined by the pump power [32,33]. With high pump power, the gain can span multiple free spectral ranges (FSRs), even for extremely small cavities [34,35], as schematically illustrated in Fig. 1(b). Hence, multiple cavity modes could emit simultaneously once their losses

are compensated by the gain. The newly generated frequency components could induce by themselves parametric oscillation, and degrade the coherence through nondegenerate four-wave mixing [34]. To avoid these detrimental effects, one could engineer the resonator's dispersion and pump it with moderate power [26–30,36]. Another strategy is to reduce the number of effective cavity modes, such as

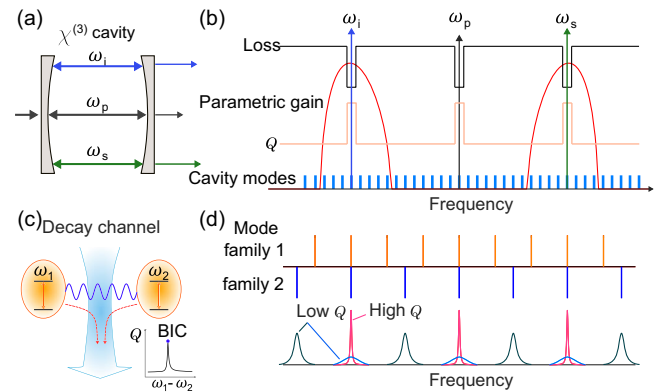


FIG. 1. Concept of H-OPO via bound states in the continuum (BICs). (a) Schematic of H-OPO. (b) Cavity quality factor ( $Q$ ) management for achieving high-efficiency H-OPO. (c) Schematic illustration of the Friedrich-Wintgen BIC. Two near degenerate resonances can be dissipatively coupled if both share a common decay channel. As a result, two supermodes are formed: one is a nondecaying bound state (high  $Q$ ) while the other one is an increased-decaying state (low  $Q$ ). (d) Realization of ( $Q$ ) engineering for cavity modes by making use of BICs in a two-mode cavity, where the high- $Q$  mode can be achieved periodically owing to the Vernier effect.

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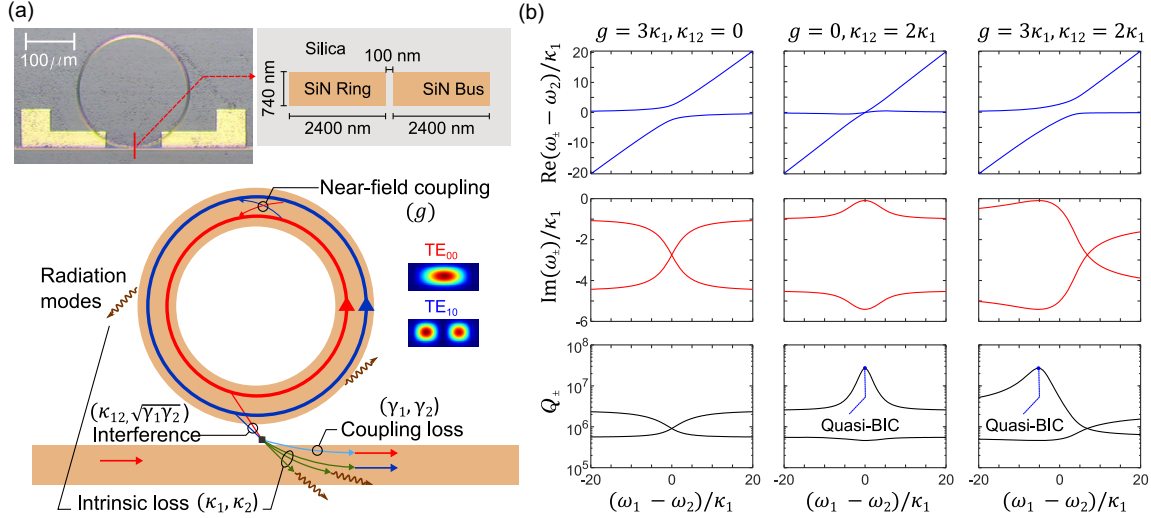


FIG. 2. BICs in a multimode microring-waveguide system. (a) Image and schematic of the system. (b) Calculated eigenfrequencies of  $\mathcal{H}$  and the corresponding  $Q$  as a function of the detuning. Parameters used here:  $\gamma_1 = \gamma_2 = 0$ ,  $\kappa_2 = 4.5\kappa_1$ ,  $\omega_1/\kappa_1 = 5 \times 10^6$ .

increasing the FSR of microresonators [28,31] or suppressing undesired modes with the aid of frequency selection elements [see Fig. 1(b)], e.g., coupled cavities and gratings [37,38]. These classical techniques, being widely used for single-frequency lasers, however, cannot be directly adapted for nonlinear optics because they are usually incompatible with the stringent demand of simultaneously attaining high- $Q$ , low-mode volume and dispersion engineering. In addition to multimode interaction, the second limiting factor of the conversion efficiency is the attainable  $Q_i/Q_c$  [26], where  $Q_{i(c)}$  is the cavity intrinsic (coupling) quality factor. Realistic microresonator-coupler systems introduce a physical limit because the coupling rate ( $\sim 1/Q_c$ ) cannot be arbitrarily high without involving additional intrinsic loss, hence, decreasing  $Q_i$  [39,40].

In this Letter, we demonstrate that the abovementioned limits can be overcome simultaneously by exploiting the concept of bound states in the continuum (BICs). As a result, high-efficiency H-OPO could be accomplished. BICs were originally proposed by von Neumann and Wigner nearly one century ago in quantum physics, and in recent years they have been extended to many other fields [41,42]. In photonics, BICs can be used to trap light and obtain high- $Q$  modes [43–48], leading to applications such as lasing [49–51], sensing [52,53], and nonlinear optics [54–59]. Here we implement the Friedrich-Wintgen BICs in an integrated multimode microresonator-waveguide system. As schematically shown in Fig. 1(c), Friedrich-Wintgen BICs can occur as a result of destructive interference if two near degenerate resonances are dissipatively coupled through a common decay channel [60,61]. Mathematically, Friedrich-Wintgen BICs are one type of singularity in anti-parity-time symmetric systems [49,62–67]. To utilize the concept of BICs for the mode number-dependent  $Q$  factor

management, we take advantage of the Vernier effect in multimode microresonators [Fig. 1(d)].

We consider an experimental system which consists of a silicon nitride ( $\text{Si}_3\text{N}_4$ ) microring resonator and an adjacent bus waveguide, as shown in Fig. 2(a). Both the ring and bus waveguide support the higher-order modes  $\text{TE}_{10}$  and  $\text{TE}_{20}$  in addition to the fundamental mode  $\text{TE}_{00}$ . The  $\text{TE}_{20}$  can be ignored in practice because its  $Q$  is much lower. Unlike most widely used microring-waveguide systems, the ring-bus gap here is very small, which allows the fundamental cavity modes to couple with the other (guided and radiation) modes in the bus waveguide besides the fundamental one; see Fig. 2(a). This results in parasitic loss for the cavity mode and an encompassing reduction in  $Q_i$  and coupling ideality [40]. The role of the bus waveguide on the intrinsic property of microcavities is not sufficiently appreciated [68], but it can have a dramatic influence, especially in multimode cavities [69–71]. In particular, the parasitic loss caused by the bus waveguide can be coherently suppressed when two near resonant cavity modes exist. In this case, Friedrich-Wintgen BICs could emerge because two cavity modes are coupled with the same decay channels. The motion of two near resonant cavity modes can be described by a Schrödinger-type equation (see Supplemental Material [72])

$$i \frac{\partial}{\partial t} |\psi\rangle = \mathcal{H} |\psi\rangle + |s\rangle, \quad (1)$$

$$\mathcal{H} = \begin{pmatrix} \omega_1 & g \\ g^* & \omega_2 \end{pmatrix} - i \begin{pmatrix} \kappa_1 & \kappa_{12} \\ \kappa_{12}^* & \kappa_2 \end{pmatrix} - i \begin{pmatrix} \gamma_1 & \sqrt{\gamma_1 \gamma_2} \\ \sqrt{\gamma_1 \gamma_2} & \gamma_2 \end{pmatrix} \quad (2)$$

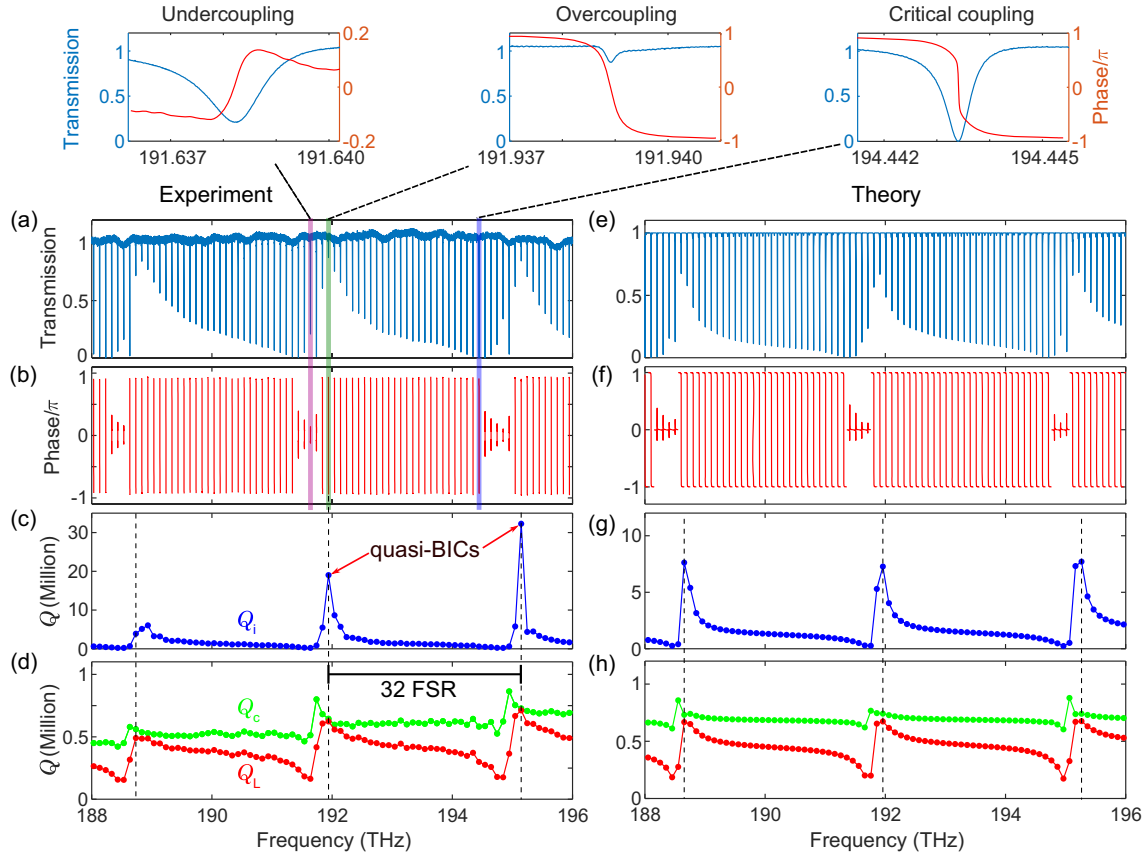


FIG. 3. Observation of BICs via spectral characterization of the system. (a) Normalized transmission scan of the microring-waveguide system. (b) Effective phase response of the system. (c) Intrinsic and (d) coupling as well as loaded  $Q$  factors for the measured resonances. Three coupling conditions: undercoupling, overcoupling, and critical coupling are enlarged in the top panel. (e)–(h) Theoretical results corresponding to the case in panels (a)–(d).

with  $|\psi\rangle = [a_1, a_2]^T$ ,  $|s\rangle = [\sqrt{2\gamma_1}, \sqrt{2\gamma_2}]^T s_{\text{in}}$ , where the  $a_{1(2)}$  are the complex amplitudes of the  $\text{TE}_{00}$  and  $\text{TE}_{10}$  cavity modes. In the first term of  $\mathcal{H}$ ,  $\omega_{1(2)}$  are the resonant frequencies in the uncoupled system, and  $g$  is the scattering-induced direct coupling coefficient between the two modes. The second term of  $\mathcal{H}$  is non-Hermitian, where  $\kappa_{1(2)}$  stand for the decay rates caused by intrinsic loss including material absorption, radiation loss, and bus-waveguide-induced parasitic loss.  $\kappa_{12}$  denotes the via-the-continuum coupling term since the two cavity modes share the same decay channels. This is the critical parameter for achieving high- $Q_i$  BIC modes. We note that the value of  $\kappa_{12}$  is restricted to  $|\kappa_{12}| < \sqrt{\kappa_1 \kappa_2}$  as not all decaying terms can be canceled by perfect destructive interference; i.e., only quasi-BICs can be attained. The third term of  $\mathcal{H}$  describes the two cavity modes coupling to the fundamental mode of the bus waveguide at rates  $\gamma_{1(2)}$ . The term  $\sqrt{\gamma_1 \gamma_2}$  plays a role similar to  $\kappa_{12}$  to generate BICs, but it acts on  $Q_c$  instead of  $Q_i$  [44]. It is worth noting that  $Q_i$  and  $Q_c$  play the same role in  $\mathcal{H}$ , but their impact on the light coupling and thus the efficiency of the nonlinear optics process is quite different.

BICs can be obtained from the eigenvalues ( $\omega_{\pm}$ ) of  $\mathcal{H}$ . The real and imaginary parts of the eigenvalues stand for the resonant frequencies and decay rates of two eigenmodes formed by the superposition of the original cavity modes. The quality factors of the two eigenmodes can be calculated by  $Q_{\pm} = |\text{Re}(\omega_{\pm}) / 2\text{Im}(\omega_{\pm})|$ . Because of coupling, both of the resonant frequencies and decay rates vary with the detuning ( $\omega_1 - \omega_2$ ). To illustrate that  $Q_i$  can be tailored as a result of BICs, we assume  $\gamma_{1(2)} = 0$  and plot the complex frequencies as a function of the detuning; see Fig. 2(b). It is shown that the scattering-induced near field direct coupling ( $g$ ) and via-the-continuum indirect coupling ( $\kappa_{12}$ ) lead to distinct effects on the eigenvalues. The former leads to the real parts of eigenvalues being avoided and imaginary parts crossed, while the latter gives rise to the opposite effect. Moreover, when only one eigenvalue becomes near purely real, a quasi-BIC is formed at the expense of the other eigenvalue becoming more lossy (its imaginary part increases). In a realistic system, both direct coupling and indirect coupling exist; thus, the interference at the coupling region is determined by both. In this scenario, quasi-BICs can still be obtained but, surprisingly at a nonzero detuning, while the  $Q$ 's also exhibit asymmetric dependence on the

detuning. These aspects will be demonstrated in the following experiment.

The bus waveguide features a tapered structure at both ends to ensure only  $TE_{00}$  can be excited and collected. The measured normalized transmission spectrum of the system is shown in Fig. 3(a). Unlike the conventional transmission spectrum of a microring-waveguide system, a doubly periodic pattern shows up, given by the nominal FSR of the fundamental mode and a periodic deletion the transmission resonance that arises from the interaction between  $TE_{00}$  and  $TE_{10}$  mode families. The period is 32 FSRs of the  $TE_{00}$  mode, which matches the Vernier frequency corresponding to the walk-off between group indices (see Supplemental Material [72]).

Although two transverse modes families are involved, it is noted that only a single clear resonance dip can be observed within each FSR dominated by  $TE_{00}$  family modes. This can be interpreted as the low- $Q_i$  eigenmodes being extremely undercoupled. Therefore, the transmission spectrum and phase response can be approximately considered as the consequence of single high- $Q_i$  eigenmodes. The measured transmittance and phase allow us to distinguish unambiguously  $Q_i$  and  $Q_c$ ; see Fig. 3 and Fig. S2 in the Supplemental Material [72].

Following the transmission spectrum, both  $Q_i$  and  $Q_c$  feature periodic patterns but with slightly shifted frequency dependence, which could be explained as the intrinsic loss and coupling loss of cavity modes correspond to different decay channels. As discussed above, due to the coexistence of direct and indirect coupling, both  $Q_i$  and  $Q_c$  as well as the transmission spectrum exhibit a Fano-like frequency dependence. The asymmetric  $Q$  distribution with respect to the pump mode further reduces the risk of mode competition in H-OPO as demonstrated in the following section. In addition to suppressing mode competition, another advantage of engineering  $Q_i$  is that the modes with highest  $Q_L$  are strongly overcoupled (top panel of Fig. 3). This counterintuitive phenomenon is especially important for achieving high-efficiency nonlinear optics phenomena, and H-OPO in particular.

The above theoretical model only considers the interaction between a pair of near resonant modes. To better describe the realistic system over a wider spectral range, we generalize the above model to four interacting modes (see Supplemental Material [72]) by including the effect that one mode from the  $TE_{00}$  family could couple to more than one mode from the  $TE_{10}$  family simultaneously and vice versa; see Figs. 3(e)–3(h). The good match between theory and experiment suggests our model captures the main underlying physics of the system.

To generate H-OPO, anomalous dispersion is required. We found the supermode's dispersion is dominated by the  $TE_{00}$  mode with mode-interaction-induced distortion (see Supplemental Material [72]). To pump this device, we use a laser located at 1561.9 nm after being amplified by an

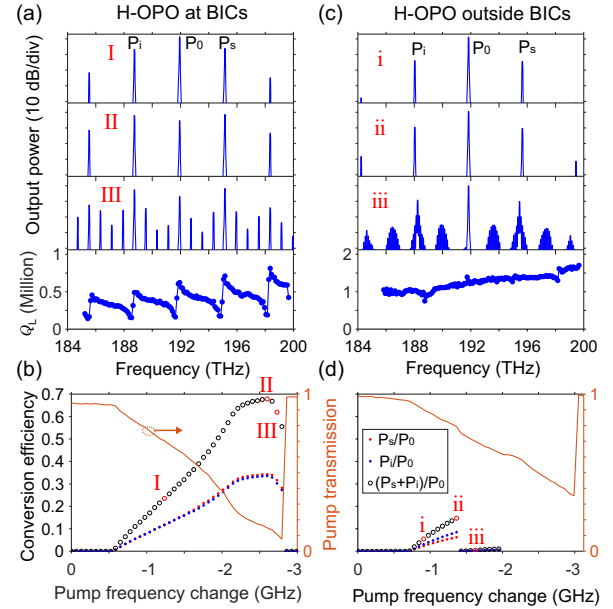


FIG. 4. Experimental demonstration of H-OPO in microresonators at and outside BICs. (a) Measured optical spectra at different pump-cavity detunings. As a reference, frequency-dependent loaded  $Q$  ( $Q_L$ ) is plotted at the bottom. (b) Calculated conversion efficiency and pump transmission as a function of the pump frequency. (c),(d) same as (a),(b) except for pumping another sample.

erbium-doped fiber amplifier. The on-chip pump power threshold of this H-OPO is  $\sim 60$  mW, and the highest conversion efficiency is attained at 200 mW. To couple pump into resonance, we decrease the laser's frequency gradually. With more pump power coupled into the microresonator, a pair of signal and idler waves are generated, exactly located at the quasi-BIC locations; see Fig. 4(a). With further decreasing the pump frequency, the power of the signal and idler increases linearly before reaching saturation [see Fig. 4(b)]. The maximum conversion efficiency  $\eta_s = (P_s + P_i)/P_0 = 68\%$  corresponding to  $\sim 70$  mW on-chip signal power. The value could be further improved if the undesired BICs (i.e., BICs modes excluding pump, signal, and idler modes) and the resultant cascaded four-wave mixing were suppressed (see Supplemental Material [72]), for example, by coupling with an auxiliary cavity [77]. By further reducing the detuning, the conversion efficiency decreases suddenly as a result of the birth of new lines, indicating the low- $Q$  modes can still be activated at high pump power. The advantage of BICs can be clearly shown if we pump another sample, which has the same geometric parameters except for a 50 nm larger ring-bus gap. Hence, it does not feature quasiperiod  $Q$  response, and the highest conversion efficiency is limited to  $< 15\%$  due to mode competition.

To conclude, we have implemented BICs in an integrated Kerr nonlinear microring resonator featuring a high-contrast quasiperiodic response in quality factor. By exploring



waveguide-assisted dissipative mode coupling in microring-waveguide system, we have generalized the spectral response and demonstrated the feasibility of boosting  $Q_i$  in high- $Q$  microresonators. Such a simple system not only enables the unwanted modes to be suppressed, but it also allows us to obtain strong overcoupling without sacrificing  $Q_i$  for desired modes. The  $Q_i$  can in fact be higher than in standard single-mode systems, resulting in unprecedented efficiency in H-OPO and high-power signal and idler waves. Besides H-OPO, the possibility to engineer the spectral response of the intrinsic quality factor of high- $Q$  microresonators can be useful for other power-efficient nonlinear optics scenarios, and the strong overcoupling (high  $Q_i/Q_c$ ) could especially facilitate the generation of squeezed or entangled states of light [8,77–80].

The raw data for this work can be accessed from Ref. [81].

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